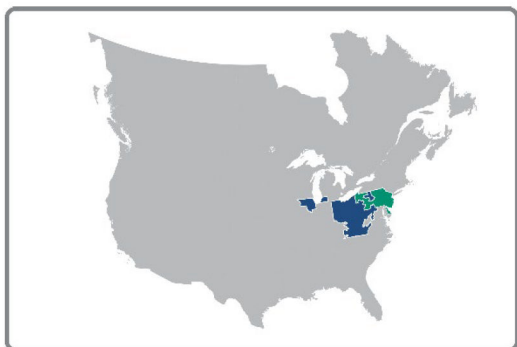


**Interface E29: SERC East <-> PJM South**

Interface Direction	2024 Summer	2024/25 Winter
SERC East -> PJM South	4,596 MW	4,963 MW
PJM South -> SERC East	4,665 MW	5,463 MW

**Interface E30: PJM West <-> PJM East**

Interface Direction	2024 Summer	2024/25 Winter
PJM West -> PJM East	4,762 MW	9,815 MW
PJM East -> PJM West	1,443 MW	166 MW

**Interface E31: PJM West <-> PJM South**

Interface Direction	2024 Summer	2024/25 Winter
PJM West -> PJM South	7,041 MW	9,035 MW
PJM South -> PJM West	5,347 MW	10,942 MW

**Interface E32: PJM East <-> PJM South**

Interface Direction	2024 Summer	2024/25 Winter
PJM East -> PJM South	5,094 MW	6,770 MW
PJM South -> PJM East	1,605 MW	4,166 MW



**Interface E33: PJM East <-> New York<sup>56</sup>**

Interface Direction	2024 Summer	2024/25 Winter
PJM East -> New York	1,356 MW	4,814 MW
New York -> PJM East	913 MW	4,019 MW

**Interface E34: Ontario -> New York**

Interface Direction	2024 Summer	2024/25 Winter
Ontario -> New York	2,286 MW	2,719 MW

<sup>56</sup> Power flow cases used to calculate these TTC values reflected the operating agreements between PJM and the New York Independent System Operator (NYISO).

**Interface E35: New York <-> New England**

Interface Direction	2024 Summer	2024/25 Winter
New York -> New England	1,303 MW	2,432 MW
New England -> New York	1,660 MW	1,359 MW

**Interface E36: Maritimes -> New England**

Interface Direction	2024 Summer	2024/25 Winter
Maritimes -> New England	1,127 MW	1,265 MW

## Québec – Eastern Interconnection Results

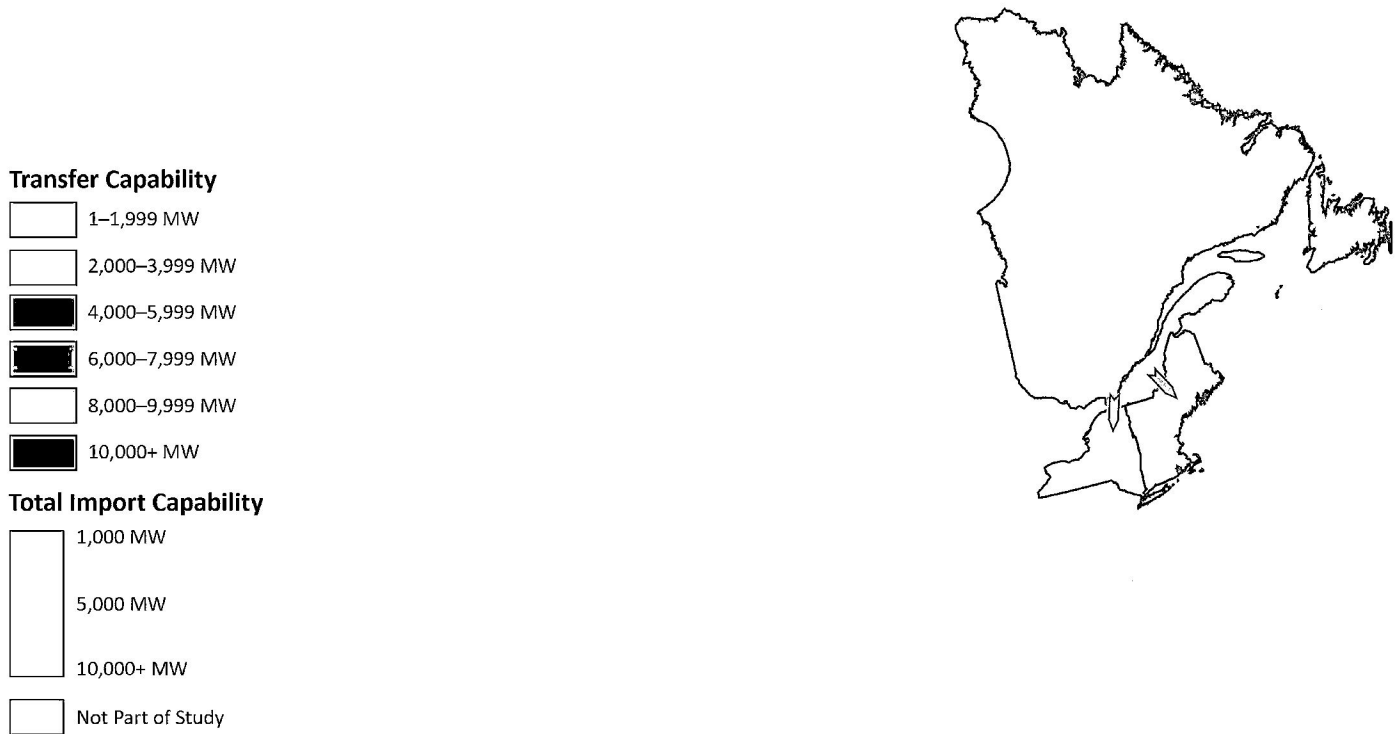
TTC results for the following interfaces are presented in this section:

**Interface QE1: Québec -> New York (dc-only)**

**Interface QE2: Québec -> New England (dc-only)**

Interfaces between Québec and Ontario and between Québec and the Maritimes will be covered in the Canadian Analysis.

**Figure 4.9** depicts the calculated transfer capabilities for the 2024 Summer case. **Figure 4.10** similarly depicts the results from the 2024/25 Winter case.



**Figure 4.9: Transfer Capability Between Québec and Eastern Interconnections (Summer)**



Figure 4.10: Transfer Capability Between Québec and Eastern Interconnections (Winter)

**Interface QE1: Québec -> New York****Special Information:** dc-only interface

Interface Direction	2024 Summer	2024/25 Winter
Québec -> New York	1,000 MW	1,000 MW

**Interface QE2: Québec -> New England****Special Information:** dc-only interface

Interface Direction	2024 Summer	2024/25 Winter
Québec -> New England	2,225 MW	2,225 MW

## Total Import Interface Results

The ITCS also analyzed an additional set of transfers into each TPR. These total import interfaces analyze the simultaneous transfers into a TPR from all its neighbors. In instances where the calculated total import interface transfer capability was lower than that from any neighboring TPR, the highest neighbor-to-neighbor results were reported to avoid understating the total import capability. The definitions of these interfaces exclude connections via dc-only interfaces, which can typically be scheduled independently. TTC results for the following interfaces are presented in this section:

**Interface WTI01: Into Washington**

**Interface WTI02: Into Oregon**

**Interface WTI03: Into California North**

**Interface WTI04: Into California South**

**Interface WTI05: Into Wasatch Front**

**Interface WTI06: Into Southwest**

**Interface WTI07: Into Front Range**

**Interface ETI01: Into SPP North**

**Interface ETI02: Into SPP South**

**Interface ETI03: Into MISO West**

**Interface ETI04: Into MISO Central**

**Interface ETI05: Into MISO South**

**Interface ETI06: Into MISO East**

**Interface ETI07: Into SERC Central**

**Interface ETI08: Into SERC Southeast**

**Interface ETI09: Into SERC Florida**

**Interface ETI10: Into SERC East**

**Interface ETI11: Into PJM West**

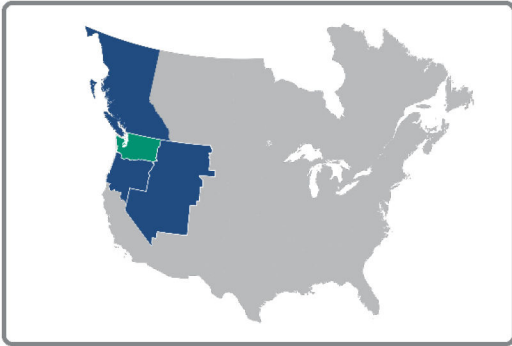
**Interface ETI12: Into PJM East**

**Interface ETI13: Into PJM South**

**Interface ETI14: Into New York**

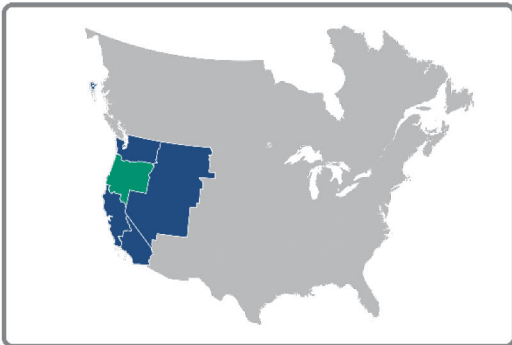
**Interface ETI15: Into New England**

### Interface WTI01: Into Washington



Interface Direction	2024 Summer	2024/25 Winter
Into Washington TTC	7,377 MW <sup>57</sup>	10,297 MW
Percentage of Peak Load	43%	50%

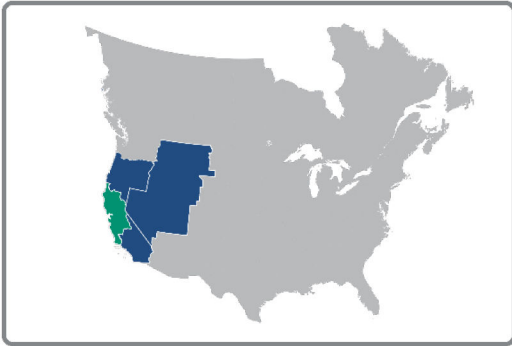
### Interface WTI02: Into Oregon



Interface Direction	2024 Summer	2024/25 Winter
Into Oregon TTC	8,004 MW	7,534 MW
dc-only interfaces	3,100 MW	3,100 MW
Total of TTC and dc-only interfaces	11,104 MW	10,634 MW
Percentage of Peak Load	92%	89%

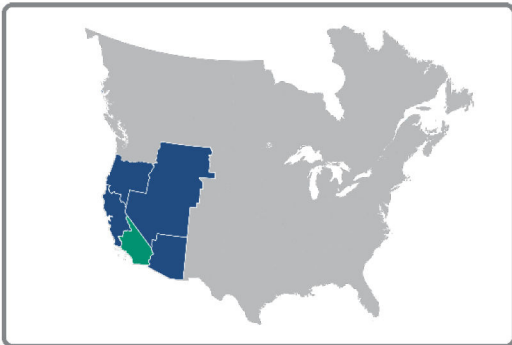
<sup>57</sup> Value is from the Wasatch Front to Washington interface, as the total import interface calculation was more limiting.

### Interface WTI03: Into California North



Interface Direction	2024 Summer	2024/25 Winter
Into California North TTC	3,972 MW <sup>58</sup>	6,631 MW
Percentage of Peak Load	14%	29%

### Interface WTI04: Into California South

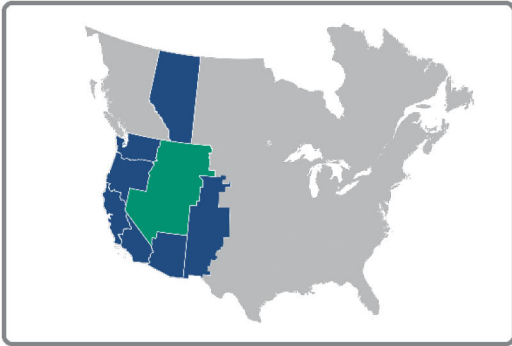


Interface Direction	2024 Summer	2024/25 Winter
Into California South TTC	7,829 MW	11,288 MW
dc-only interfaces	3,220 MW	3,220 MW
Total of TTC and dc-only interfaces	11,049 MW	14,508 MW
Percentage of Peak Load	28%	69%

<sup>58</sup> Value is from the Oregon to California North interface, as the total import interface calculation was more limiting.

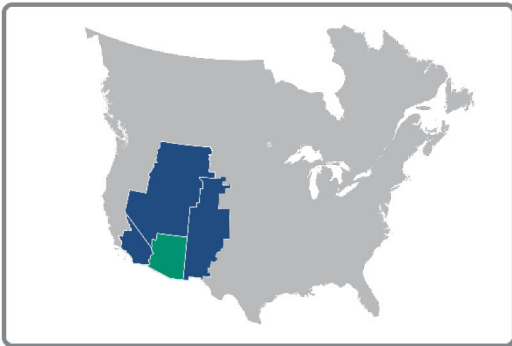


### Interface WTI05: Into Wasatch Front



Interface Direction	2024 Summer	2024/25 Winter
Into Wasatch Front TTC	5,965 MW <sup>59</sup>	5,558 MW
dc-only interfaces	200 MW	200 MW
Total of TTC and dc-only interfaces	6,165 MW	5,758 MW
Percentage of Peak Load	23%	35%

### Interface WTI06: Into Southwest



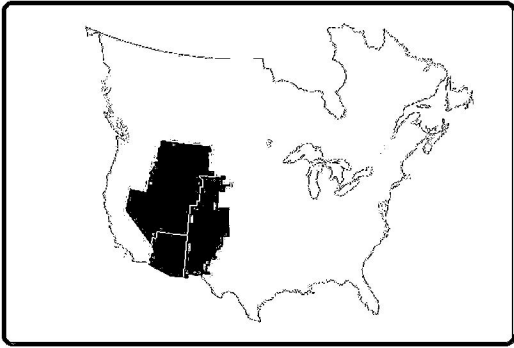
Interface Direction	2024 Summer	2024/25 Winter
Into Southwest TTC	5,247 MW <sup>60</sup>	8,470 MW <sup>61</sup>
Percentage of Peak Load	22%	66%

<sup>59</sup> Value is from the California South to Wasatch Front interface, as the total import interface calculation was more limiting.

<sup>60</sup> Value is from the California South to Southwest interface, as the total import interface calculation was more limiting.

<sup>61</sup> Value is from the California South to Southwest interface, as the total import interface calculation was more limiting.

## Interface WTI07: Into Front Range

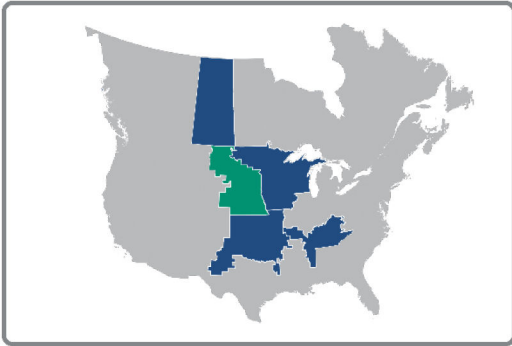


Interface	Direction	2024 Summer	2024/25 Winter
Into Front Range	TTC	3,284 MW <sup>62</sup>	3,751 MW <sup>63</sup>
dc-only	interfaces	920 MW	920 MW
Total of TTC and dc-only interfaces		4,204 MW	4,671 MW
Percentage of Peak Load		21%	30%

<sup>62</sup> Value is from the Southwest to Front Range interface, as the total import interface calculation was more limiting.

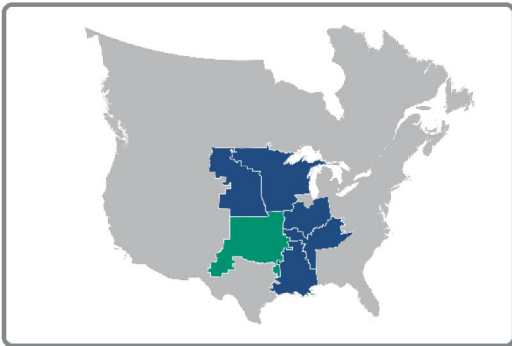
<sup>63</sup> Value is from the Southwest to Front Range interface, as the total import interface calculation was more limiting.

### Interface ETI01: Into SPP North



Interface Direction	2024 Summer	2024/25 Winter
Into SPP North TTC	2,209 MW <sup>64</sup>	663 MW <sup>65</sup>
dc-only interfaces	660 MW	660 MW
Total of TTC and dc-only interfaces	2,869 MW	1,323 MW
Percentage of Peak Load	21%	11%

### Interface ETI02: Into SPP South



Interface Direction	2024 Summer	2024/25 Winter
Into SPP South TTC	5,042 MW <sup>66</sup>	6,445 MW <sup>67</sup>
dc-only interfaces	1,230 MW	1,230 MW
Total of TTC and dc-only interfaces	6,272 MW	7,675 MW
Percentage of Peak Load	13%	20%

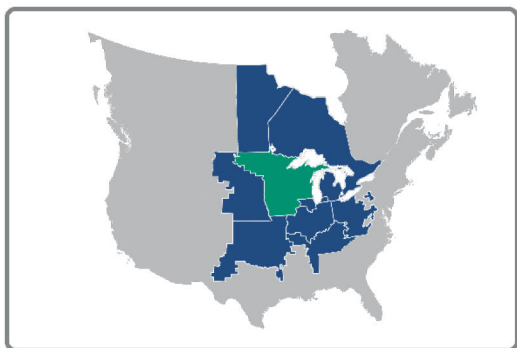
<sup>64</sup> Value is from the MISO West to SPP North interface, as the total import interface calculation was more limiting.

<sup>65</sup> Value is from the Saskatchewan to SPP North interface, as the total import interface calculation was more limiting.

<sup>66</sup> Value is from the SERC Central to SPP South interface, as the total import interface calculation was more limiting.

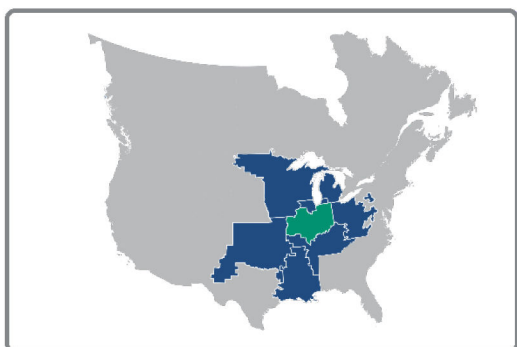
<sup>67</sup> Value is from the SERC Central to SPP South interface, as the total import interface calculation was more limiting.

### Interface ETI03: Into MISO West



Interface Direction	2024 Summer	2024/25 Winter
Into MISO West TTC	7,791 MW <sup>68</sup>	9,086 MW <sup>69</sup>
dc-only interfaces	160 MW	160 MW
Total of TTC and dc-only interfaces	7,951 MW	9,246 MW
Percentage of Peak Load	19%	26%

### Interface ETI04: Into MISO Central



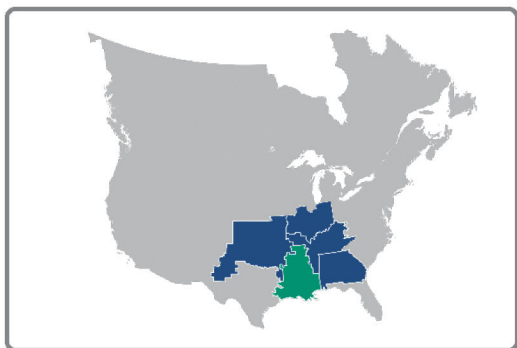
Interface Direction	2024 Summer	2024/25 Winter
Into MISO Central TTC	12,714 MW	20,449 MW <sup>70</sup>
Percentage of Peak Load	35%	63%

<sup>68</sup> Value is from the PJM West to MISO West interface, as the total import interface calculation was more limiting.

<sup>69</sup> Value is from the PJM West to MISO West interface, as the total import interface calculation was more limiting.

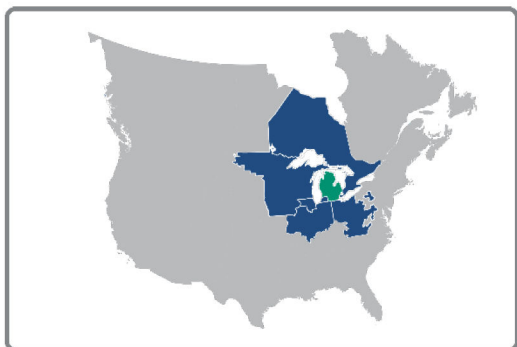
<sup>70</sup> Value is from the PJM West to MISO Central interface, as the total import interface calculation was more limiting.

## Interface ETI05: Into MISO South



Interface Direction	2024 Summer	2024/25 Winter
Into MISO South TTC	4,295 MW <sup>71</sup>	4,336 MW <sup>72</sup>
Percentage of Peak Load	12%	13%

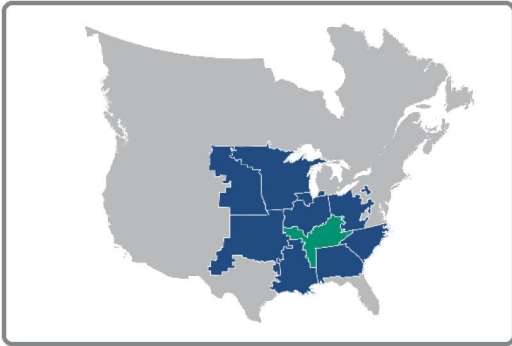
## Interface ETI06: Into MISO East



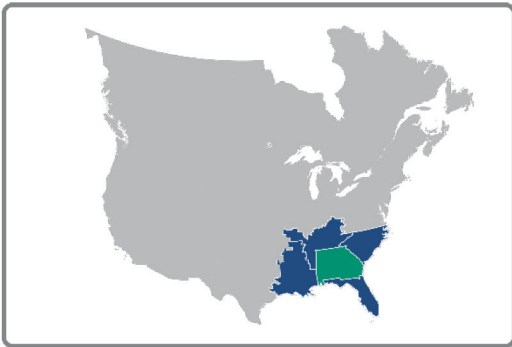
Interface Direction	2024 Summer	2024/25 Winter
Into MISO East TTC	5,139 MW	7,019 MW
dc-only interfaces	160 MW	160 MW
Total of TTC and dc-only interfaces	5,299 MW	7,179 MW
Percentage of Peak Load	25%	44%

<sup>71</sup> Value is from the SPP South to MISO South interface, as the total import interface calculation was more limiting.

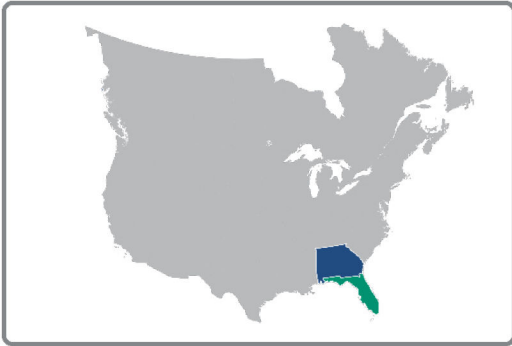
<sup>72</sup> Value is from the SPP South to MISO South interface, as the total import interface calculation was more limiting.

**Interface ETI07: Into SERC Central**

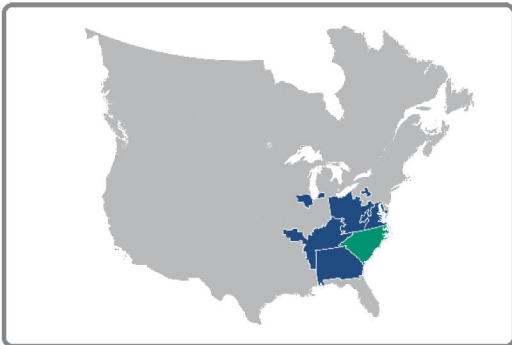
Interface Direction	2024 Summer	2024/25 Winter
Into SERC Central TTC	6,878 MW	8,443 MW
Percentage of Peak Load	15%	18%

**Interface ETI08: Into SERC Southeast**

Interface Direction	2024 Summer	2024/25 Winter
Into SERC Southeast TTC	4,900 MW	6,525 MW
Percentage of Peak Load	11%	15%

**Interface ETI09: Into SERC Florida**

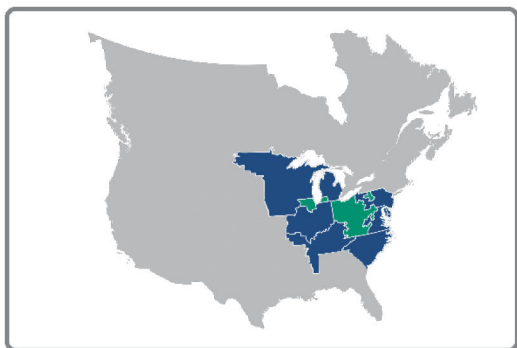
Interface Direction	2024 Summer	2024/25 Winter
Into SERC Florida TTC	2,958 MW	1,807 MW
Percentage of Peak Load	6%	4%

**Interface ETI10: Into SERC East**

Interface Direction	2024 Summer	2024/25 Winter
Into SERC East TTC	6,959 MW	5,463 MW <sup>73</sup>
Percentage of Peak Load	16%	12%

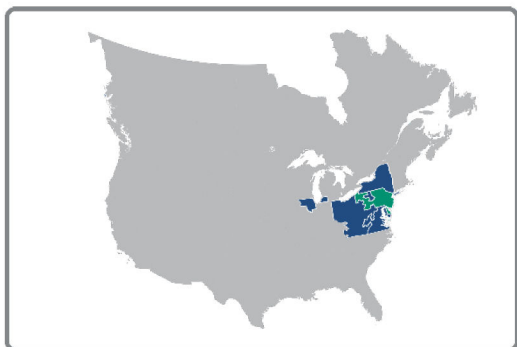
<sup>73</sup> Value is from PJM South to SERC East interface, as the total import interface calculation was more limiting.

## Interface ETI11: Into PJM West



Interface Direction	2024 Summer	2024/25 Winter
Into PJM West TTC	21,773 MW	10,942 MW <sup>74</sup>
Percentage of Peak Load	28%	16%

## Interface ETI12: Into PJM East



Interface Direction	2024 Summer	2024/25 Winter
Into PJM East TTC	4,762 MW <sup>75</sup>	9,815 MW <sup>76</sup>
Percentage of Peak Load	11%	28%

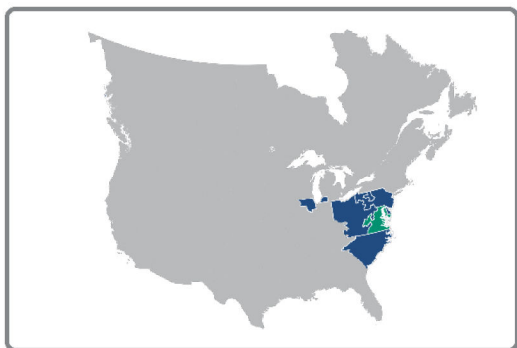
<sup>74</sup> Value is from the PJM South to PJM West interface, as the total import interface calculation was more limiting.

<sup>75</sup> Value is from the PJM West to PJM East interface, as the total import interface calculation was more limiting.

<sup>76</sup> Value is from the PJM West to PJM East interface, as the total import interface calculation was more limiting.

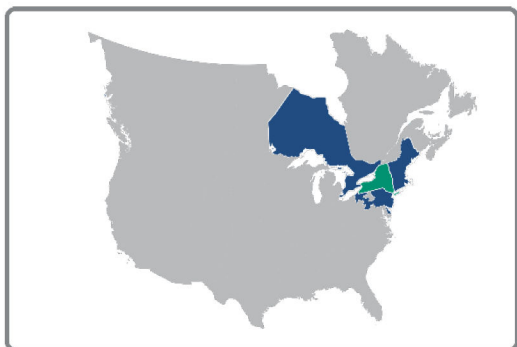


### Interface ETI13: Into PJM South



Interface Direction	2024 Summer	2024/25 Winter
Into PJM South TTC	9,578 MW	9,035 MW <sup>77</sup>
Percentage of Peak Load	28%	27%

### Interface ETI14: Into New York



Interface Direction	2024 Summer	2024/25 Winter
Into New York TTC	2,802 MW	4,814 MW <sup>78</sup>
dc-only interfaces	1,000 MW	1,000 MW
Total of TTC and dc-only interfaces	3,802 MW	5,814 MW
Percentage of Peak Load	12%	24%

<sup>77</sup> Value is from the PJM West to PJM South interface, as the total import interface calculation was more limiting.

<sup>78</sup> Value is from the PJM East to New York interface, as the total import interface calculation was more limiting.

Interface ETI15: Into New England



InterfaceDirection	2024 Summer	2024/25 Winter
Into New England TTC	2,313 MW	3,033 MW
dc-only interfaces	2,225 MW	2,225 MW
Total of TTC and dc-only interfaces	4,538 MW	5,258 MW
Percentage of Peak Load	19%	25%

## Supplemental Results Between Order 1000 Areas

The ITCS analyzed an additional set of transfers between areas defined in FERC's Order 1000 (see [Figure 4.11](#)). While these larger geographic areas were not be used for the purpose of determining prudent additions, the current transfer capability results are provided for completeness. While the Los Angeles Department of Water & Power (LADWP) is part of WestConnect, for the purposes of this study, LADWP was included as part of CAISO due to its geographic location within California. Where results were previously presented, they are not repeated here. TTC results for the following interfaces are presented in this section:

**Interface W1001: British Columbia -> Northern Grid**

**Interface W1002: Alberta -> Northern Grid**

**Interface W1003: Northern Grid <-> California ISO**

**Interface W1004: Northern Grid <-> West Connect**

**Interface W1005: California ISO <-> West Connect**

**Interface E1001: Saskatchewan -> SPP**

**Interface E1002: SPP <-> MISO**

**Interface E1003: SPP <-> SERTP**

**Interface E1004: Manitoba -> MISO**

**Interface E1005: Ontario -> MISO**

**Interface E1006: MISO <-> PJM**

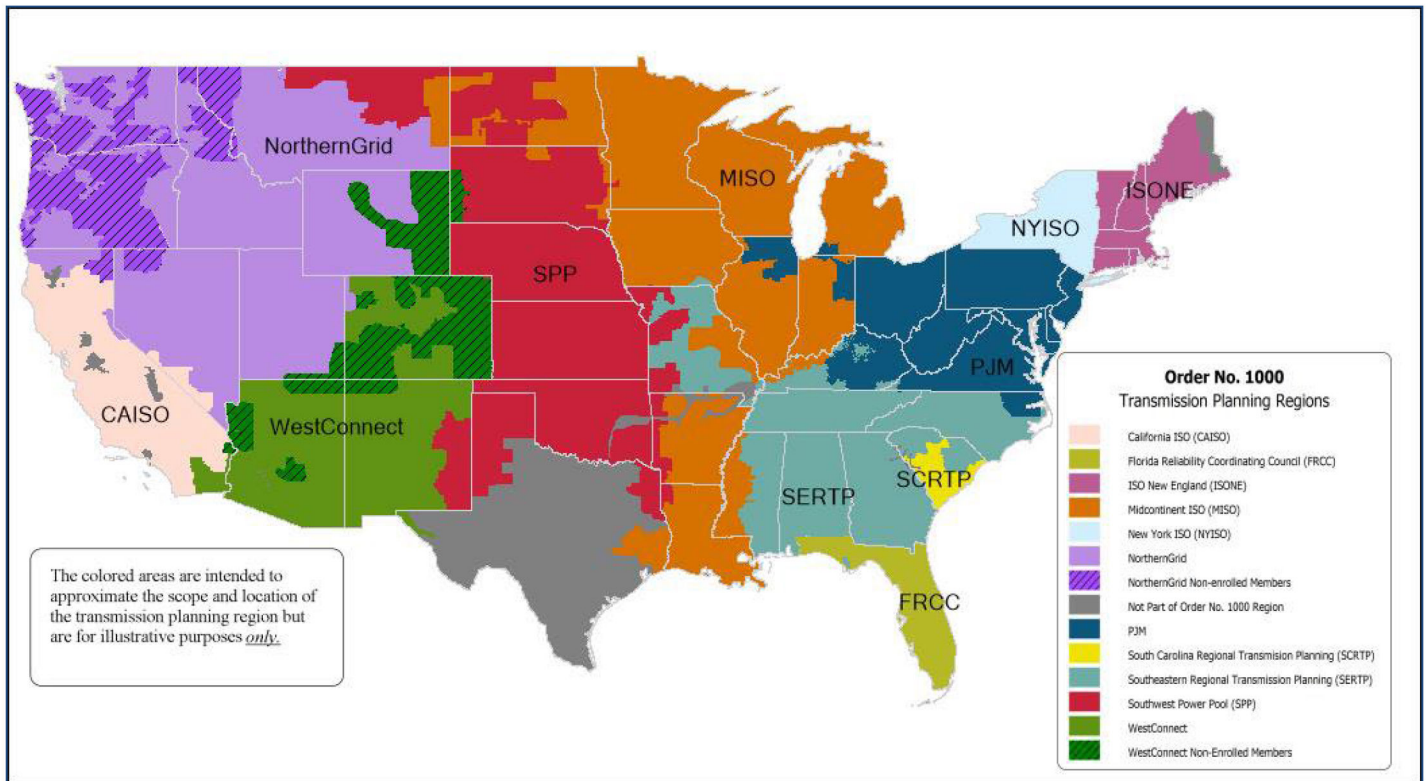
**Interface E1007: MISO <-> SERTP**

**Interface E1008: SERTP <-> PJM**

**Interface E1009: SERTP <-> SCRTP**

**Interface E1010: SERTP <-> FRCC**

**Interface E1011: PJM <-> New York**



**Figure 4.11: Areas Defined in FERC Order 1000<sup>79</sup>**

<sup>79</sup> An electronic version of this map can be found [here](https://www.ferc.gov) (ferc.gov)

**Interface W1001: British Columbia -> Northern Grid**

Interface Direction	2024 Summer	2024/25 Winter
British Columbia -> Northern Grid	2,435 MW	2,164 MW

**Interface W1002: Alberta -> Northern Grid**

Interface Direction	2024 Summer	2024/25 Winter
Alberta -> Northern Grid	981 MW	1,286 MW

**Interface W1003: Northern Grid <-> California ISO**

Interface Direction	2024 Summer	2024/25 Winter
Northern Grid -> California ISO	4,140 MW	8,705 MW
California ISO -> Northern Grid	1,985 MW	5,208 MW

**Interface W1004: Northern Grid <-> West Connect**

Interface Direction	2024 Summer	2024/25 Winter
Northern Grid -> West Connect	2,842 MW	3,326 MW
West Connect -> Northern Grid	5,710 MW	1,865 MW

**Interface W1005: California ISO <-> West Connect**

Interface Direction	2024 Summer	2024/25 Winter
California ISO -> West Connect	2,534 MW	2,375 MW
West Connect -> California ISO	2,967 MW	3,912 MW

**Interface E1001: Saskatchewan -> SPP**

Interface Direction	2024 Summer	2024/25 Winter
Saskatchewan -> SPP	0 MW	665 MW

**Interface E1002: SPP <-> MISO**

Interface Direction	2024 Summer	2024/25 Winter
SPP -> MISO	7,058 MW	1,513 MW
MISO -> SPP	5,308 MW	6,403 MW

**Interface E1003: SPP <-> SERTP**

Interface Direction	2024 Summer	2024/25 Winter
SPP -> SERTP	4,857 MW	2,814 MW
SERTP -> SPP	2,822 MW	6,324 MW

**Interface E1004: Manitoba -> MISO**

Interface Direction	2024 Summer	2024/25 Winter
Manitoba -> MISO	3,058 MW	3,058 MW

**Interface E1005: Ontario -> MISO**

Interface Direction	2024 Summer	2024/25 Winter
Ontario -> MISO	2,419 MW	1,834 MW

**Interface E1006: MISO <-> PJM**

Interface Direction	2024 Summer	2024/25 Winter
MISO -> PJM	5,593 MW	12,552 MW
PJM -> MISO	9,146 MW	10,771 MW

**Interface E1007: MISO <-> SERTP**

Interface Direction	2024 Summer	2024/25 Winter
MISO -> SERTP	6,976 MW	9,543 MW
SERTP -> MISO	0 MW	9,801 MW

**Interface E1008: SERTP <-> PJM**

Interface Direction	2024 Summer	2024/25 Winter
SERTP -> PJM	8,609 MW	9,782 MW
PJM -> SERTP	7,704 MW	7,905 MW

**Interface E1009: SERTP <-> SCRTP**

Interface Direction	2024 Summer	2024/25 Winter
SERTP -> SCRTP	1,767 MW	1,948 MW
SCRTP -> SERTP	2,415 MW	2,335 MW

**Interface E1010: SERTP <-> FRCC**

Interface Direction	2024 Summer	2024/25 Winter
SERTP -> FRCC	2,918 MW	1,803 MW
FRCC -> SERTP	1,058 MW	0 MW

**Interface E1011: PJM <-> New York<sup>80</sup>**

Interface Direction	2024 Summer	2024/25 Winter
PJM -> New York	635 MW	858 MW
New York -> PJM	3,136 MW	3,394 MW

<sup>80</sup> Power flow cases used to calculate these TTC values reflected the operating agreements between PJM and the New York Independent System Operator (NYISO).



## Chapter 5: Prudent Additions (Part 2) Inputs

### Selected Weather Years

Part 2 used a two-pronged approach for inputs and assumptions to study a variety of conditions across 12 different weather years. This approach combined synthetic, modeled datasets from 2007 to 2013<sup>81</sup> with historical, actual data from 2019<sup>82</sup> to 2023, as shown in [Figure 5.1](#). This combination increased the number of weather years available for analysis and helped overcome the limitations in both types of datasets.



**Figure 5.1: Two-Pronged Approach for Historical Weather Data**

*Note: The hourly energy margin analysis did not simulate historical operations, but rather applied historical weather year data to simulate future grid operations under similar conditions.*

The synthetic approach used historical weather data to estimate load and resource availability if those same weather conditions were to occur again in the future. The historic approach used historical measured data for load, as well as wind and solar resource output, from recent years and scaled it appropriately to represent future conditions. More detail on these approaches is shown in [Appendix A](#), including sources from the National Renewable Energy Laboratory (NREL), the Energy Information Administration (EIA), and FERC forms.

By evaluating all hours of the year across 12 weather years, Part 2 inherently evaluates resource availability, load, and opportunities for energy transfers between TPRs during both normal and extreme weather over more than 105,000 hours. A list of known extreme weather events embedded in the Part 2 analysis include:

- Intense Florida Cold Wave, 2010
- Intense Southern Cold Wave, 2011
- Western Wide Area Heat Domes, 2020-2022
- Winter Storm Uri, 2021
- Winter Storm Elliott, 2022
- Midwest Wind Drought, 2023
- Western and Midwest Heat Waves, 2023
- Northeast Heat Wave, 2023

While using 12 weather years provides a diverse set of extreme weather conditions to evaluate, it should not be interpreted as representative of all possible conditions. If, for example, one TPR does not show a resource deficiency in the 12 weather years evaluated, it does not mean that it is robust against all weather conditions. This is important when considering when and where resource deficiencies arise and when additional transfer capability can mitigate these risks.

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**The studied weather years should not be interpreted as representative of all possible extreme weather conditions.**

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<sup>81</sup> 2013 is the last year with available National Renewable Energy Laboratory (NREL) Wind Toolkit data.

<sup>82</sup> 2019 is the first full calendar year with available Energy Information Administration (EIA) Form EIA-930 data.



## Load Assumptions

A range of load conditions across the grid was studied, time-synchronized and correlated with respect to weather. Of particular interest is the load, which may be much higher during extreme weather conditions than forecasted in the 2023 LTRA data submissions.<sup>83</sup> A combination of historical load (2019-2023) and synthetic load (2007-2013) was used to capture a range of hourly variability in load for each TPR. Recent historical loads were used to capture recent weather events and associated load behavior as they occurred, using the EIA 930 hourly demand data. Synthetic loads were used to supplement the range of load behavior during weather conditions that may not be represented in the recent five-year history, with the further benefit of isolating electrification impacts and economic growth in the load profiles. The hourly profiles were then scaled to the LTRA forecasted load on both an energy and seasonal peak basis. Additional detail on the data source and load scaling done for the load profiles is available in **Appendix B**.

The overall goal of scaling the weather year profiles was to provide hourly profiles that reflect the varying magnitude and timing of peak load across each TPR that were scaled to forecasted annual energy and peak demand targets. The result of the scaling effort maintains the underlying weather variability but increases the overall peak and energy values to align with the LTRA, maintaining variations in seasonal peak load across weather years. This approach was reviewed by the ITCS Advisory Group. Tables that show the resulting peak loads are available in **Appendix C**.

## Resource Mix

Resource portfolios for the Part 2 analysis, aligned with the 2023 LTRA, included existing generators, retirements, Tier 1 resources, and a portion of Tier 2 resource additions to create portfolios for 2024 and 2033.

The LTRA is a NERC assessment of supply and demand on a peak-hour basis, evaluating the winter and summer seasonal reserve margins for North American areas, considering the expected contribution of each resource type during the peak load hours. In Part 2 of the ITCS, however, the LTRA resource mix was evaluated across all hours of the year, and multiple weather years by varying hourly loads and resource supply.

Two study years were the starting points for evaluation in Part 2:

- **2024 Case:** Included all existing resources, plus certain retirements and Tier 1 resource additions online by the summer season, the 2024 peak load, and the annual energy forecast from the LTRA.
- **2033 Case:** Included all existing resources, plus certain retirements and Tier 1 resource additions expected by 2033, the 2033 peak load, and the annual energy forecast from the LTRA. Further, new resources were added to TPRs that retired capacity in the LTRA by also adding a portion of Tier 2 and Tier 3 resources.

Unit-level information was used to distinguish between fuel types and to map generation capacity to each TPR from the larger LTRA assessment areas. The analysis considered resource availability across aggregated fuel types, including natural gas (single fuel and dual-fuel), coal, oil, nuclear, hydro, land-based wind, offshore wind, utility-scale solar, behind-the-meter solar, pumped storage hydro, and battery storage. It did not perform any unit-specific modeling but captured variability in resource availability at the aggregate level based on historical performance and synthetic weather conditions.

Winter and summer seasonal capacity ratings were used to represent installed capacity for each TPR by fuel type, except for solar and wind resources, where nameplate capacity was used. Using the LTRA winter and summer capacity ratings for 2024 and 2033 ensures that capacity mixes in Part 2 include retirements and units unavailable for other reasons in a manner consistent with the LTRA.

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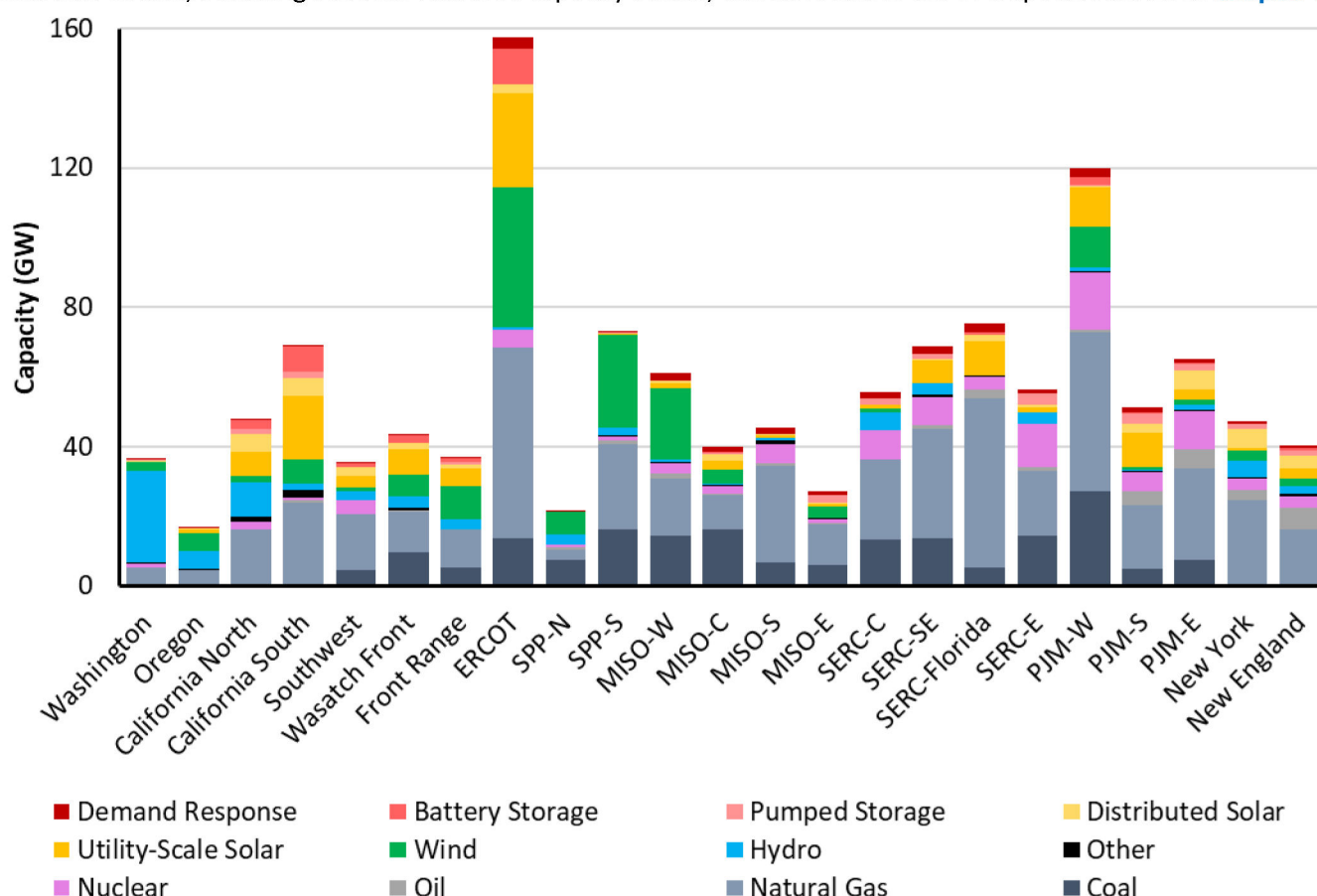
<sup>83</sup> The 2023 LTRA can be found [here](#).

Resources were assigned to TPRs based on their geographic locations. Contractual obligations between generation units and load in a different TPR were not considered. This is an appropriate modeling choice for determining the amount of transfer capability needed to transfer energy from one TPR to another. As such, energy deficiency as modeled does not imply that an entity is failing to meet its resource adequacy obligations.

The LTRA generator and load data was aligned to the TPRs used in Part 1 for both existing and future resource additions. For example, the SPP LTRA assessment area was divided into SPP-N and SPP-S TPRs so that the energy analysis used the same breakdown as Part 1. Given the differences between resource and transmission planning, some resource differences between Part 1 and Part 2 analysis were expected. Additional detail can be found in [Appendix D](#).

## 2024 Resource Mix

**Figure 5.2** shows the winter capacity of the 2024 resource mix by TPR and type based on the LTRA data forms. Additional details, including summer resource capacity values, can be found in the TPR-specific tables in [Chapter 9](#).



**Figure 5.2: Capacity, Existing + Tier 1 Resources (2024 Case)**

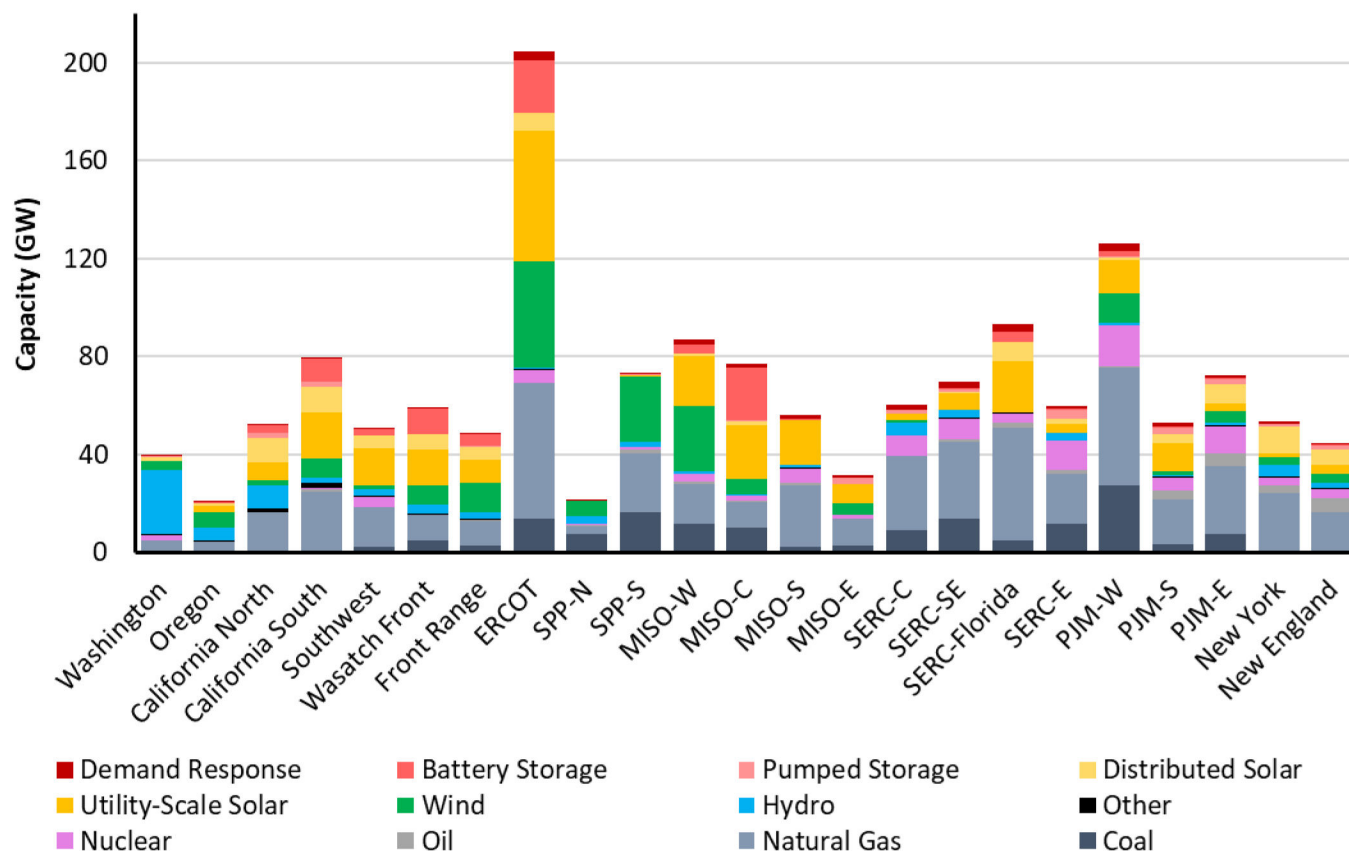
## 2033 Resource Mix

The capacity mix for the 2033 study year required adjustments relative to using the existing plus Tier 1 resources provided in the LTRA data forms. Tier 1 resources generally represent plants that are under construction or have high confidence to be online. An initial review revealed that Tier 1 additions are insufficient alone to meet 2033 load growth expectations because Tier 1 resources are inherently more near-term than the 10-year-out case. However, review of the Tier 2 and Tier 3 resources, which include less certain and more speculative resource additions, revealed different application of these tiers across the country. In some cases, the entire generator interconnection queue is

included in these tiers, whereas in other cases, no resources were identified as Tier 2 or 3. This disparity necessitated a different approach to ensure that the future capacity mix was reasonable and applied in a consistent manner.

To this end, 2033 capacity mixes were developed based on the reported retirements in that TPR and the types of resources identified in its Tier 2 and 3 lists. If no Tier 2 or 3 resources existed, then Tier 1 was used. The Part 2 study used this “Replace Retirements” scenario. For every MW of retired certain capacity, an equivalent amount of accredited capacity was added. Additional detail regarding the 2033 “Replace Retirements” scenario, including the resulting resource additions, can be found in [Appendix E](#). This approach was reviewed by the ITCS Advisory Group.

**Figure 5.3** shows the 2033 winter capacity mix by TPR and technology type based on the LTRA data forms.



**Figure 5.3: Capacity, Existing + Tier 1 + Replace Retirements (2033 Case)**

## Resource Modeling

Additional detail regarding modeling of certain resource types is noted below. These modeling details were reviewed by the ITCS Advisory Group.

### Wind and Solar Modeling

Wind and solar resources were modeled using a combination of historical and synthetic weather year data to represent the hourly energy variability within each TPR. Both datasets described in this section result in hourly capacity factor values for utility scale solar (UPV), distributed behind-the-meter solar (BTM PV), land-based wind (LBW), and offshore wind (OSW). While the underlying datasets for the historical and synthetic weather years are different, as discussed in [Appendix A](#), both produced a capacity-weighted profile for each resource type within each TPR, normalized to the installed capacity. As a result, this capacity-weighted profile can be used for different levels of renewable resource capacity. In a few cases, historical data was supplemented with synthetic data for the same weather years, or historical and synthetic data was used to recreate weather years not covered directly by the

historical or synthetic record based on temperature and wind-speed relationships. The steps taken to create each set of profiles and descriptions of the underlying data for each weather year profile are provided in **Appendix F**.

### **Hydro Resource Availability**

Hydro resources were modeled with monthly maximum availability factors based on historical observations. While they are renewable resources, the availability of hydro is relatively uncorrelated with wind, solar, and load conditions and affected by longer inter-annual cycles in water availability. Also, hydro resources may be limited in generating at maximum capacity for several reasons in addition to typical generator maintenance and forced outages. These factors include water levels on rivers and constraints due to reservoir levels. To account for these factors on hydro generating potential, a monthly maximum availability was created for each TPR based on historical data, thereby limiting the maximum generation that hydro resources could contribute. No limitations on monthly or annual energy production were applied and it was assumed that the maximum output seen in historical records was the limiting factor for hydro resources.

In Canadian TPRs, like Hydro Québec, where hydro generation regularly serves most or all of the demand throughout much of the year, historical generation data does not fully represent the actual availability of hydro resources, especially during lower load months. Discussion with these entities, where needed, resulted in modifications to the monthly hydro capacity used in the simulations to better reflect resource availability.

### **Thermal Generator Outage Modeling**

Thermal generators were aggregated by TPR and fuel type to account for daily fluctuations in available capacity. Thermal capacity was aggregated by up to eight fuel types in each TPR, resulting in 290 unique capacity aggregations across the North American BPS. These aggregations were done to represent the total, fleet-wide resource availability, rather than individual generator outage sampling traditionally done in resource adequacy modeling.

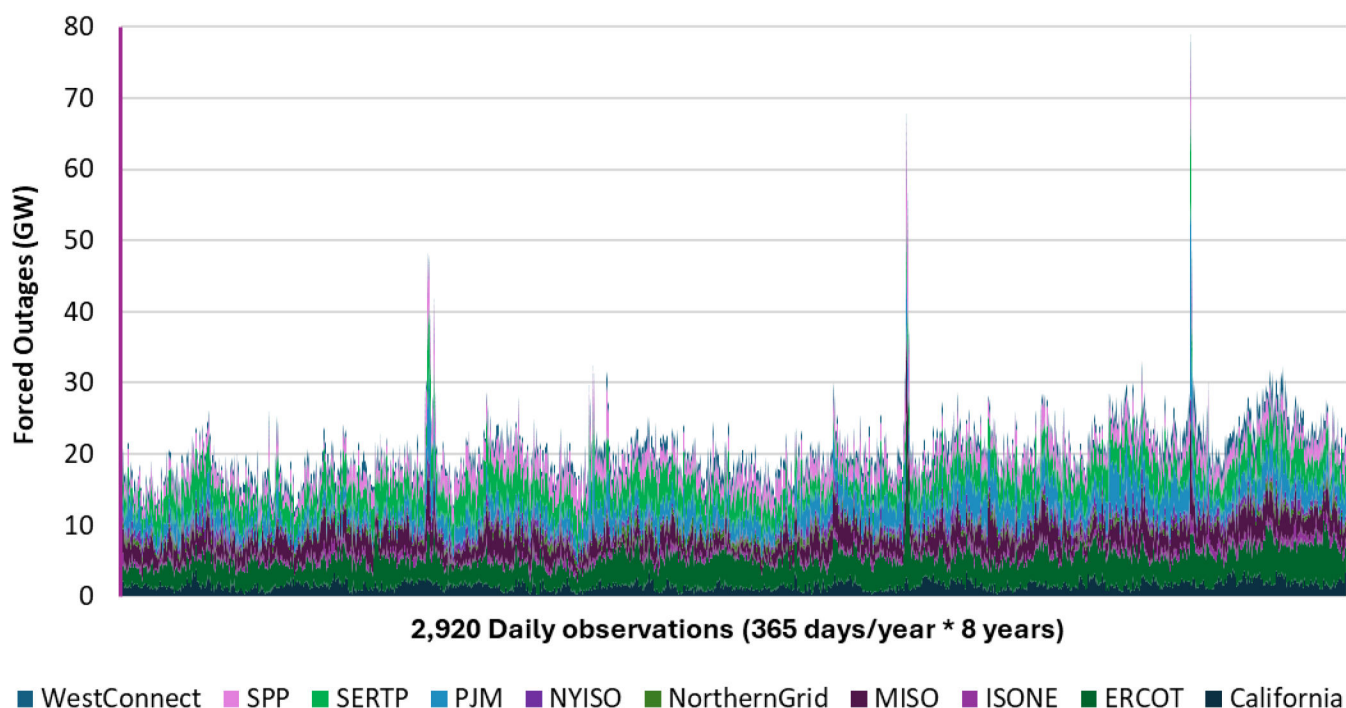
Each of the 290 aggregated resource types was then modeled to reflect daily fluctuations in available capacity, accounting for fleet-wide maintenance and forced outages, weather-dependent forced outages, and seasonal maintenance schedules. Ambient derates were reflected for summer and winter based on the associated capacity values provided in the 2023 LTRA data forms.

### ***Forced Outages and Derates***

**Figure 5.4** shows the aggregated capacity of forced outages across the United States on a daily basis from 2016 to 2023, derived from available GADS<sup>84</sup> data. Additional detail regarding these calculations and application can be found in **Appendix G**. The analysis shows daily and seasonal variation in forced outages, but most importantly, extreme spikes in forced outages observed during the January 2018 winter event, Winter Storm Uri (February 2021) and Winter Storm Elliott (December 2022). Generator outage modeling was intentionally done on an aggregated fleet-wide basis to capture correlated outages across large areas.

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<sup>84</sup> Generating Availability Data System, a NERC database that includes outages and derates



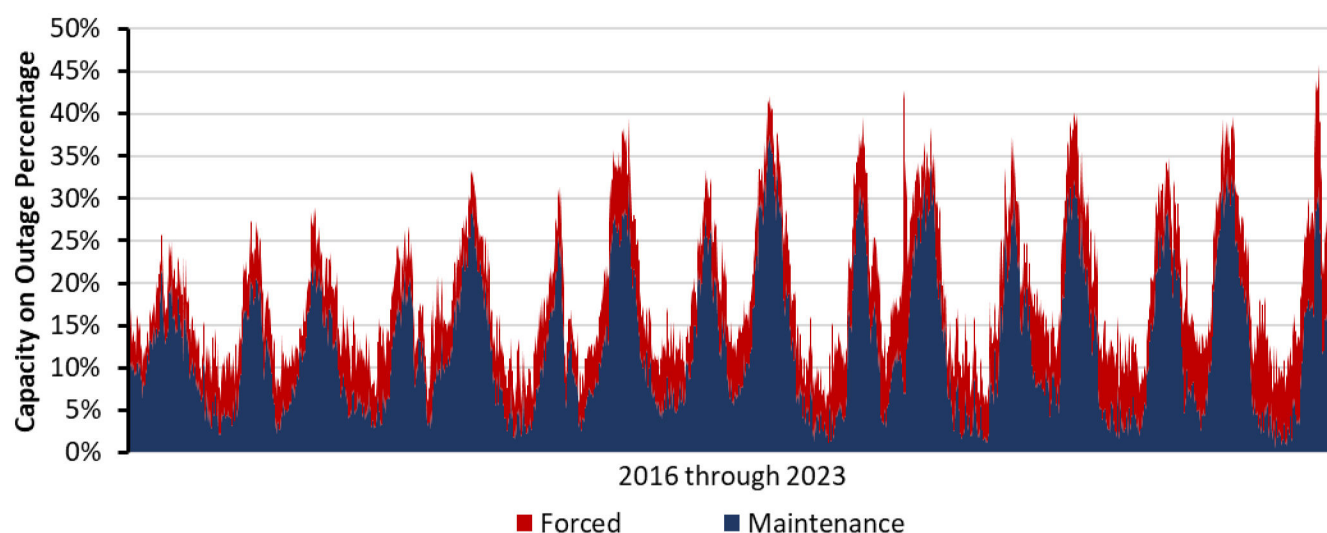
**Figure 5.4: Total Daily U.S. Forced Outages and Derates (in GW)**

#### *Planned and Maintenance Outages and Derates*

Similar to the forced outage rate modeling, planned and maintenance outages and derates were modeled based on historical GADS data, by day, by TPR, and by fuel type. This data in aggregate was converted to an average capacity on outage per day, as a percentage of Net Maximum Capacity.

An example of the combined capacity on outage (Forced Outages and Maintenance) is provided in [Figure 5.5](#) for a single TPR and single fuel type (natural gas, single fuel). This figure clearly shows the seasonal increases in maintenance during the shoulder seasons (spring and fall) and the potential for increased capacity on outage during extreme weather events (e.g., Winter Storm Uri). While the forced outages were higher during this event, less capacity was on planned maintenance because it occurred during the winter season.





**Figure 5.5: Forced and Planned Outages for Single Fuel Natural Gas (% of Capacity)**

### *ERCOT Winterization Mandate*

Due to the statewide mandate<sup>85</sup> in Texas directing winterization measures to be implemented across the generation fleet, discussion with the Regional Entity (Texas RE) resulted in a modification to ERCOT resource availability relative to the historical GADS data. Efforts resulting from the winterization mandate are expected to improve thermal resource availability during extreme cold weather events to be no less than 85% of the winter rating. This adjustment was made to the input data for the months of December, January, and February. The winterization case is used as the starting point for ERCOT and is reflected in the energy margin analysis and recommended additions in [Chapter 7](#). A comparison of the results with and without the winterization mandate are shown for ERCOT as a sensitivity in [Chapter 8](#).

### **Storage Modeling**

Storage resources, both pumped storage hydro and battery storage, were modeled as two distinct units for each TPR. Information regarding installed capacity for each resource type for existing and future capacity builds was taken from the 2023 LTRA. Since information on the duration of each storage plant was limited or not available, it was assumed that pumped storage hydro would have 12 hours of duration and battery storage was four hours<sup>86</sup> based on trends and available battery storage information from the EIA Form 860.

Storage resources were allowed to charge dynamically within the model to create hourly profiles of charging (adding load) and discharging (generation), subject to round-trip efficiency losses of 30% for pumped storage hydro and 13% for battery storage resources. Storage resources were scheduled to arbitrage hourly energy margins, based on the resource scheduling method described in [Chapter 6](#). In doing so, storage was charged during periods of high energy margins (surplus resources) and discharged during periods of lower energy margins. Furthermore, the storage resources did not optimize imports/exports between TPRs, although during grid stress events, storage resources were allowed to recharge via imports if available.

### **Demand Response Modeling**

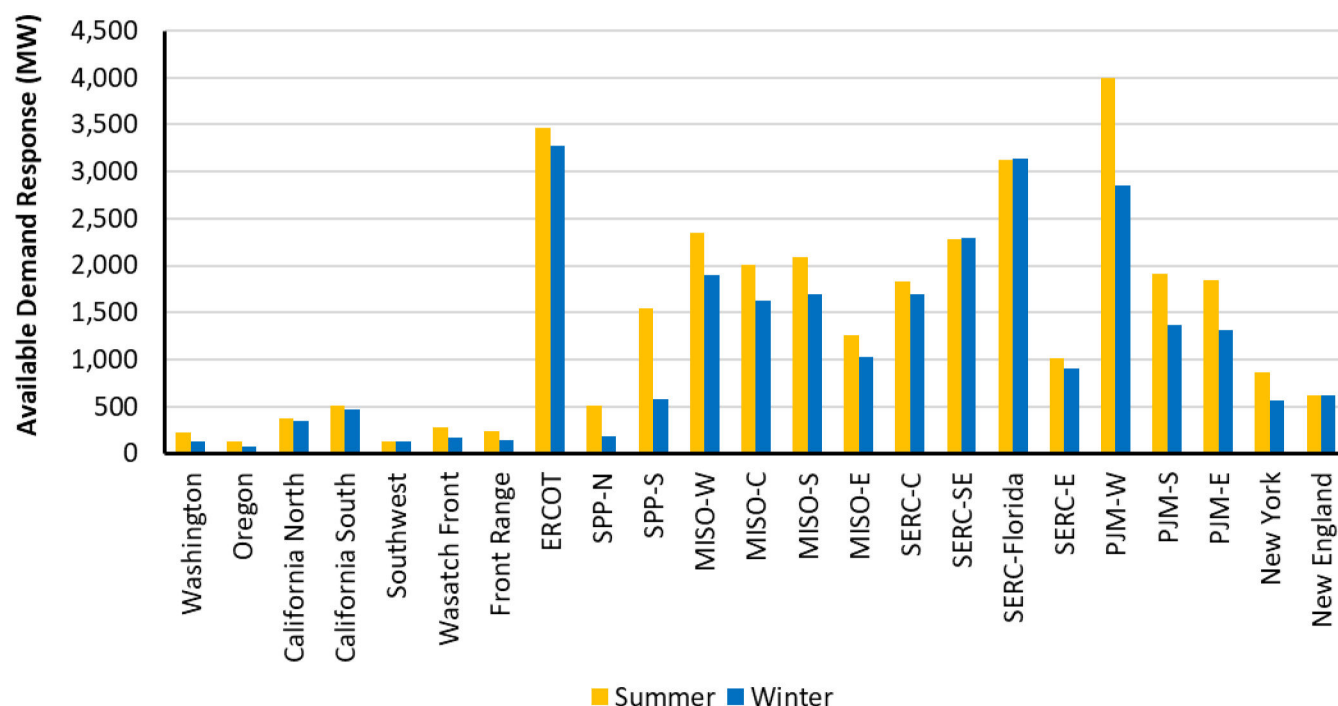
Demand response resources were also included in the model as a supply-side resource that could be dynamically scheduled by the model to mitigate resource deficiency events. Similar to storage resources, demand response was

<sup>85</sup> Texas Public Utilities Commission Weather Emergency Preparedness (adopted September 29, 2022) standards can be found [here](#) and [here](#) (2 documents).

<sup>86</sup> Three hours was used for ERCOT due to lower duration of existing and planned resources.

modeled assuming both capacity (MW) and energy (MWh) limitations but did not assume any round-trip energy losses or payback required. Demand response was modeled only after energy transfers between TPRs.

Demand response capacity was based on the LTRA Form A data submissions, “Controllable and Dispatchable Demand Response – Available,” which represents the estimated demand response available during seasonal peak demand periods. While both “Total” and “Available” demand response capacity values were reported, the “Available” resource potential, shown in [Figure 5.6](#), was used to represent any assumed derates due to non-performance when called on. For LTRA assessment areas with multiple TPRs, demand response was allocated proportionally to load.



**Figure 5.6: Available Demand Response by TPR**

Energy constraints were also assumed for demand response resources to ensure that they were deployed sparingly. All demand response resources were modeled with a maximum of three hours per day up to the seasonal capacity. These hourly “per call” constraints were converted into energy constraints, meaning a demand response resource could choose to spread its capacity over six hours in a day, if needed, but would have to do so by deploying only a portion of the total capacity. Lastly, demand response resources were considered the resource of last resort to avoid load shedding, deploying only after all local resources and imports were fully exhausted.

## Chapter 6: Prudent Additions (Part 2) Process

Using the multi-year, hourly, correlated, time-synchronized dataset for load, wind, solar, and thermal resource availability described in [Chapter 5](#), the prudent additions process identified instances of resource deficiency and evaluated where additional transfer capability would improve energy adequacy. This data-driven process evaluated specific time periods where extreme weather may impact loads and resource availability in one TPR, but neighboring TPRs may have surplus energy available, thus capturing geographic diversity. This approach considered where resource deficiencies occurred, which interfaces were at their limits, and which adjacent TPRs had available energy to export. Specifically, a six-step process was used to identify and quantify prudent additions to transfer capability, each of which is discussed further in this section:

1. Identify hours of resource deficiency
2. Quantify the maximum resource deficiency
3. Prioritize constrained interfaces
4. Allocate additional transfer capability
5. Iterate until resource deficiencies are mitigated
6. Finalize prudent level of transfer capability

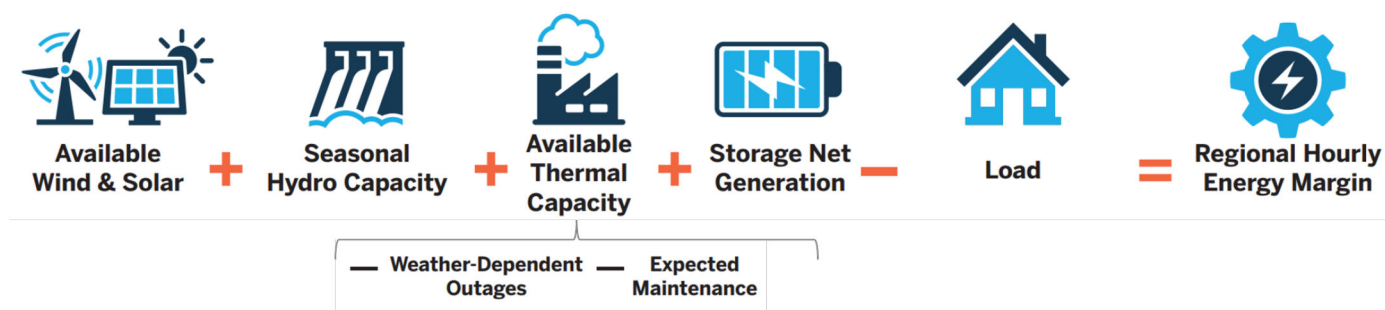


### Identify

#### Step 1: Identify Hours of Resource Deficiency

The prudent additions process begins with the calculation of the hourly energy margin for each TPR. Unlike traditional planning reserve margins that evaluate the supply and demand during expected peak load conditions, the energy margin analysis is an 8,760-hour chronological assessment of each TPR's load and availability of resources. The energy margin analysis, therefore, provides an assessment of a TPR's potential surplus or deficit across each hour of the year. In addition, the energy margin analysis was conducted over 12 weather years, allowing for fluctuations in load, wind, solar, and thermal resources based on weather conditions, along with seasonal hydro availability.

The energy margin analysis captures the impacts of variable renewables, scheduling of storage resources, expected outage conditions, and load levels associated with specific weather conditions. The formula in [Figure 6.1](#) below further characterizes the hourly energy margin, followed by an explanation of each property. All properties vary hourly except for available thermal capacity (daily variation) and hydro capacity (monthly variation).

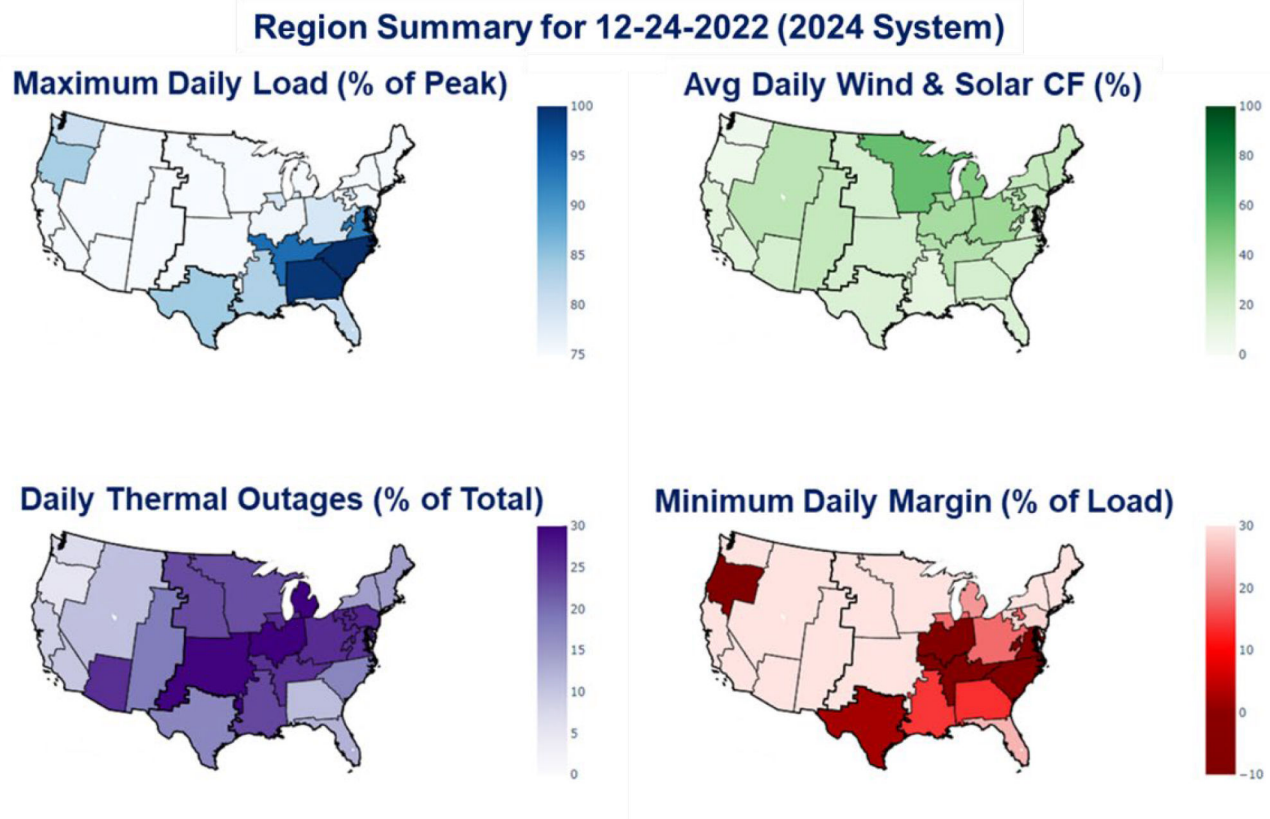


**Figure 6.1: Hourly Energy Margin Calculation**

Source: Energy Systems Integration Group, 2024



The results of the energy margin analysis provide an *hourly, time-synchronized, locational, and consistent dataset*, allowing for direct comparisons between TPRs. When one TPR has a low hourly energy margin (i.e., a low supply of resources relative to demand), the analysis considers the availability of resources and load in all neighboring TPRs simultaneously. Additional detail regarding the energy margin analysis can be found in [Appendix H](#). Below, [Figure 6.2](#) shows an example of the time-synchronized load, renewable output, weather-dependent outages, and hourly energy margin.



**Figure 6.2: Example of Correlated Load, Renewable Output, Weather-Dependent Outages, and Hourly Energy Margin**

### Resource Scheduling Method

The hourly energy margin is then used to model the available energy across the entire North American BPS for all 12 weather years. This is done to consider the energy adequacy in each TPR, with and without transfers from neighboring TPRs. To isolate reliability needs, resources are first scheduled within a TPR to serve its load before relying on neighboring TPRs. This method allowed for appropriate charge and discharge patterns for energy-limited resources like storage and demand response. The primary reason for using this dispatch model was to ensure that any recommended additions to transfer capability are to improve energy adequacy, and thereby strengthen reliability, rather than for policy or economic objectives, such as minimizing overall production cost. Operating costs are intentionally not considered for resources in this model. Instead, an operating constraint will increase the scarcity weighting factor in a TPR as the margin between supply and demand becomes tighter. This ensures that the dispatch decisions are driven by relative surplus or scarcity rather than resource dispatch costs. Additional information regarding the dispatch model and scarcity weighting factor calculations can be found in [Appendix I](#).

## Margin Levels

Margins were applied to each TPR's hourly load to account for study uncertainty and operational practices. Unlike a planning reserve margin, which is often denoted in terms of peak demand, these margins are applied to all hours of the year, in an equal percentage of demand.

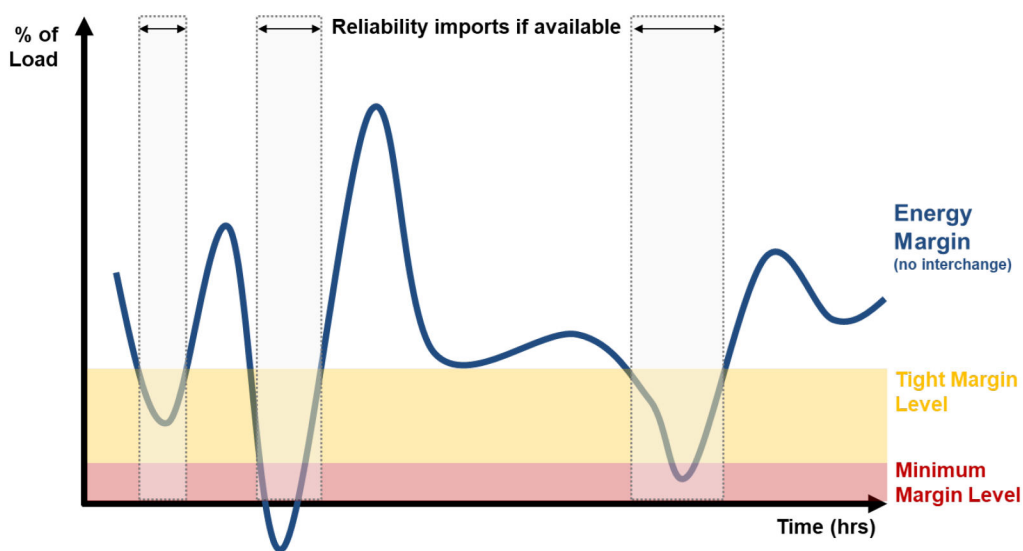
The first threshold, the **tight margin level**, determines when a TPR will seek to import energy. This threshold, applied across all hours, was set at 10% of the TPR's load based on observed projected daily reserves. This level was discussed and endorsed by the ITCS Advisory Group.

The second margin, the **minimum margin level**, determines when a TPR will incur unserved energy (load reduction) if additional resources or imports are unavailable. Following multiple discussions with, and feedback from, the ITCS Advisory Group, this value was set at 3% of the TPR's load. An additional sensitivity was conducted using a 6% minimum margin level.

A more detailed rationale for these levels is provided in [Appendix J](#).

## Energy Transfers

**Figure 6.3** illustrates the relationship between the hourly energy margin and the conditions under which a TPR may import or export energy. This is crucial for understanding how energy transfers are modeled.



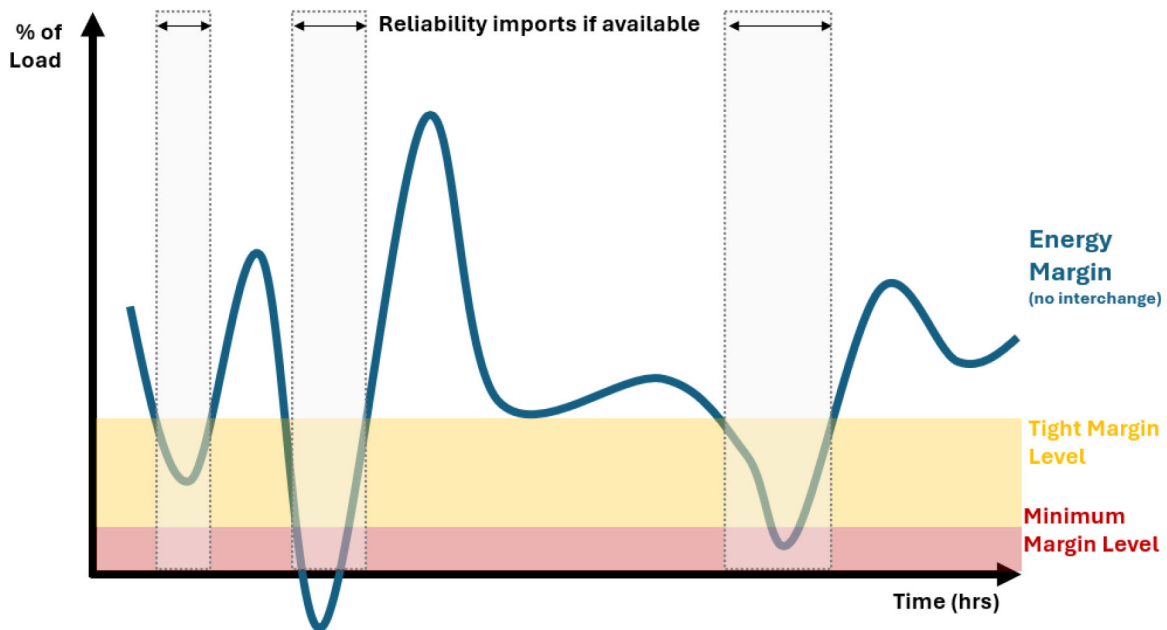
**Figure 6.3: Illustrative Example of the Hourly Energy Margin and Reserve Levels**

The line represents the hourly energy margin for a TPR, showing the difference between available energy supply and the TPR's load, fluctuating due to changes in supply and demand discussed previously. Two different threshold levels are also shown:

- The **tight margin level** (yellow zone) indicates the desired margin under normal conditions. When the energy margin is above this zone, the TPR is in surplus and is a good candidate to export energy to other TPRs that may need additional energy. When the energy margin is within this level, the TPR has enough capacity to meet its load, but uncertainty in the forecast (resource mix, load levels, weather impacts, outages, etc.) may warrant additional energy imports if available. The tight margin level dictates **when** TPRs will import energy from their neighbors, if it is available.
- The **minimum margin level** (red zone) marks the minimum permissible threshold, below which the TPR faces a resource deficiency. In this red zone, it is assumed that the TPR may experience load reduction if energy

imports from neighbors are unavailable. This retention of reserves is consistent with normal operating practices, where a Balancing Authority will continue to hold reserves even if involuntary load shed is underway to safeguard the system from cascading or widespread outages that would adversely affect overall BPS reliability. The minimum margin level determines when, and to what extent, new transfer capability is considered to mitigate the energy deficiency.

Visualized another way, [Figure 6.4](#) shows how the model will attempt to import energy any time that a TPR's energy margin drops below the tight margin level.



**Figure 6.4: Illustrative Example when Imports Occur in the Model**

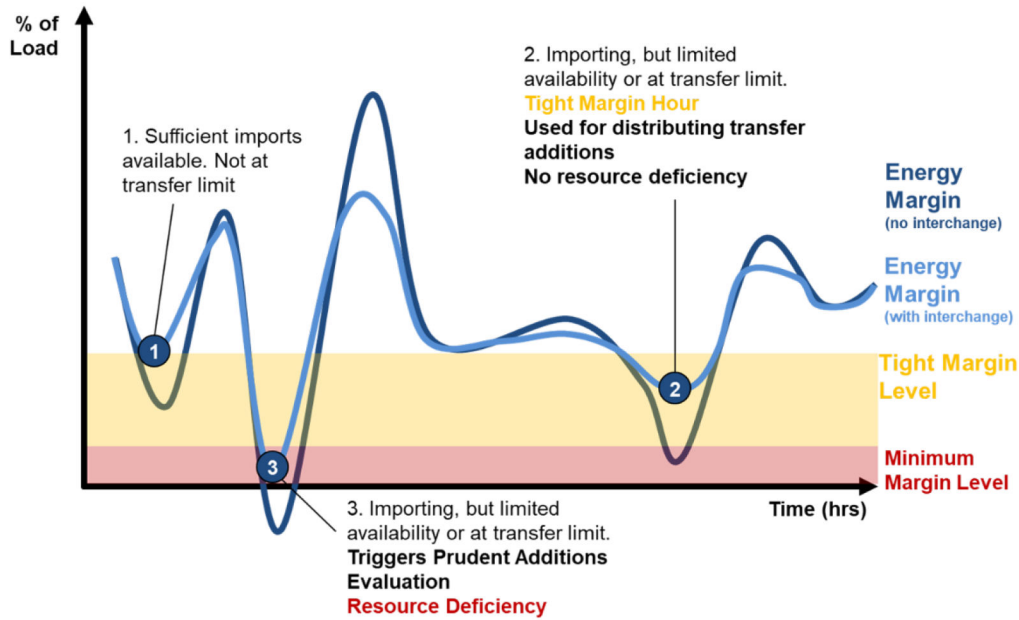
The method for determining transfers between TPRs relies heavily on the tight margin level and minimum margin level. While each TPR initially uses its available resources to meet demand and associated margin, as the energy margin tightens, its scarcity weighting factor increases to reflect the growing need for additional resources.

When a TPR falls below the tight margin level, it begins to import energy from neighboring TPRs. The decision on which neighbor to import from is based on the respective scarcity weighting factors of those neighbors. This ensures that imports are sourced from neighbors with the most surplus capacity (i.e., the lowest scarcity weighting factor). If sufficient imports are unavailable due to transmission interface limits and/or lack of available resources, the TPR may temporarily violate the tight margin level but will still maintain a minimum margin level. This is referred to as a tight margin hour.

If a TPR's energy margin drops to the minimum margin level after exhausting available imports and demand response, the model will decrease the load served, resulting in unserved energy. This is referred to as a resource deficiency hour.

[Figure 6.5](#) shows the hourly energy margin after interchange is scheduled (light blue line). Exports to neighbors are shown as a reduction in the hourly energy margin when a TPR has relative surplus, while imports are shown as an increase in the hourly energy margin when a TPR drops below the tight margin level.





**Figure 6.5: Illustrative Example Showing Impacts of Imported Energy**

## Metrics

Three important points can be considered in [Figure 6.5](#) above:

- **Point 1** indicates that a TPR, in isolation, is below the tight margin level but there is sufficient transfer capability to import energy from its neighbors to maintain the tight margin level. This represents an **interchange hour**. Because the imports allow the TPR to get back to its tight margin level, transfer capability is sufficient and not limiting.
- **Point 2** indicates that a TPR is unable to get back to the tight margin level even with imports. At this point, the transfer capability is insufficient and limited and/or neighboring TPRs do not have sufficient resources to share. This point is referred to as a **tight margin hour**.
- **Point 3** indicates that a TPR is unable to get back to the minimum margin level even with imports from its neighbors. In this example the model will reduce load in the TPR rather than dropping below the minimum margin level, resulting in unserved energy. This is referred to as a **resource deficiency hour** and is used to trigger prudent additions evaluation as described in later steps.

The model performed the above analysis for all TPRs across all hours over 12 weather years. The calculated metrics, which include the hourly energy margin, are shown in [Table 6.1](#).

**Table 6.1: Calculated Metrics**

Metric	Units	Description
<b>Energy Margin</b>	MW or %	Tracks the hourly energy margin of available capacity relative to load over the course of the year. Quantified in both MW and percent and summarized to show average, minimum, or number of times below a threshold.
<b>Interchange Hour</b>	Hours, MW, or MWh	Quantifies the number of hours, maximum flow, or total energy when a TPR imports to keep its hourly energy margin at the tight margin level. This metric calculates the frequency and quantity of imports for each TPR.
<b>Tight Margin Hour</b>	Hours, MW, or MWh	Quantifies the number of hours in a year, maximum deficit (MW), or total deficit (MWh) when a TPR is below the tight margin level (10%). <sup>87</sup> This metric quantifies how often the transfer capability is insufficient due to interface limit <u>or</u> due to lack of resources.
<b>Resource Deficiency Hour</b>	Hours, MW, or MWh	Quantifies the number of hours in a year, maximum deficit (MW), or total deficit (MWh) when a TPR is at the minimum margin level (3%) <sup>88</sup> and experiences unserved energy.
<b>Hours Congested</b>	Hours	Quantifies the number of hours in a year where the transfer capability is at the maximum import capacity. This metric quantifies how often an interface's transfer capability is insufficient.



## Quantify

## Step 2: Quantify Maximum Resource Deficiency

In Step 1, the energy margin analysis quantified the frequency, magnitude, and duration of energy deficiency for each TPR. To illustrate the output of this process, a portion of the 2033 energy margin analysis results are shown in [Table 6.2](#) below. Specifically, this table shows the yearly maximum resource deficiency (in MW) for each of the 12 weather years, with winter deficiencies highlighted in blue and summer deficiencies shown in orange. The full set of energy margin analysis results can be found in [Chapter 7](#).

**Table 6.2: Maximum Resource Deficiency (MW) for Select TPRs by Weather Year (2033 Case)**

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Max Resource Deficiency
California North	0	0	0	0	0	0	0	0	0	0	3,211	0	3,211
ERCOT	1,361	0	0	9,400	0	0	0	8,977	14,853	18,926	14,321	12,108	18,926
SPP-N	0	0	0	0	0	0	0	0	0	155	0	0	155
SPP-S	0	0	0	0	0	0	0	0	0	4,137	0	0	4,137
MISO-S	0	0	560	0	629	0	0	0	0	0	0	0	629
MISO-E	0	0	0	0	1,676	0	0	0	5,715	979	0	0	5,715
SERC-Florida	0	0	1,030	1,152	0	0	0	0	0	0	0	0	1,152
SERC-E	0	0	0	0	0	0	0	0	0	0	5,849	0	5,849
PJM-S	0	0	0	0	0	0	0	0	0	0	4,147	0	4,147
New York	0	81	0	3,244	1,748	2,631	1,229	0	0	0	0	3,729	3,729
New England	0	0	0	85	0	984	68	0	0	0	0	0	984

The largest yearly maximum resource deficiency identified across all 12 weather years is known as the maximum resource deficiency. This value is a critical input to Step 4, described later.

<sup>87</sup> As a reminder, further discussion on the tight margin level can be found in [Appendix J](#).

<sup>88</sup> As a reminder, further discussion on the minimum margin level can be found in [Appendix J](#).



### Prioritize

## Step 3: Prioritize Constrained Interfaces

Step 3 focuses on identifying constrained interfaces. After determining which TPRs are in deficit (Step 1) and to what extent (Step 2), the third step is to determine which specific interfaces are constrained during tight margin hours by calculating the number of hours that individual interfaces, including total import interfaces, are transferring energy at their TTC. This is quantified as hours congested across each interface. Additionally, the model calculates the difference between the scarcity weighting factors of each TPR when imports occur and the transmission interface is at its limit. This measures the relative resource surplus between potential sending (exporting) TPRs that could help the receiving (importing) TPR.

The difference between the scarcity weighting factors of the importing and exporting TPRs helps quantify the best candidates for increased transfer capability. In cases where the total import interface is constrained, the difference between the scarcity weighting factor between each pair of TPRs is still quantified and is used as the measure to increase both the individual interface capability and the total import interface limit.

As an example, the 2033 energy margin analysis showed SERC-E in a resource deficiency during WY2022 (Winter Storm Elliott). Neighbors PJM-W, SERC-C, and SERC-SE are already exporting resources to SERC-E, which has reached its transfer capability. During this event, SERC-SE has the lowest scarcity weighting factor, followed by PJM-W, then SERC-C. The scarcity weighting factors indicate that transfer capability should be prioritized from SERC-SE, followed by PJM-W, then SERC-C. The interface from PJM-S, which is not at its limit, would not benefit from additional transfer capability during this event, as it has no surplus resources available.

This calculation is repeated for all TPRs for all tight margin hours.

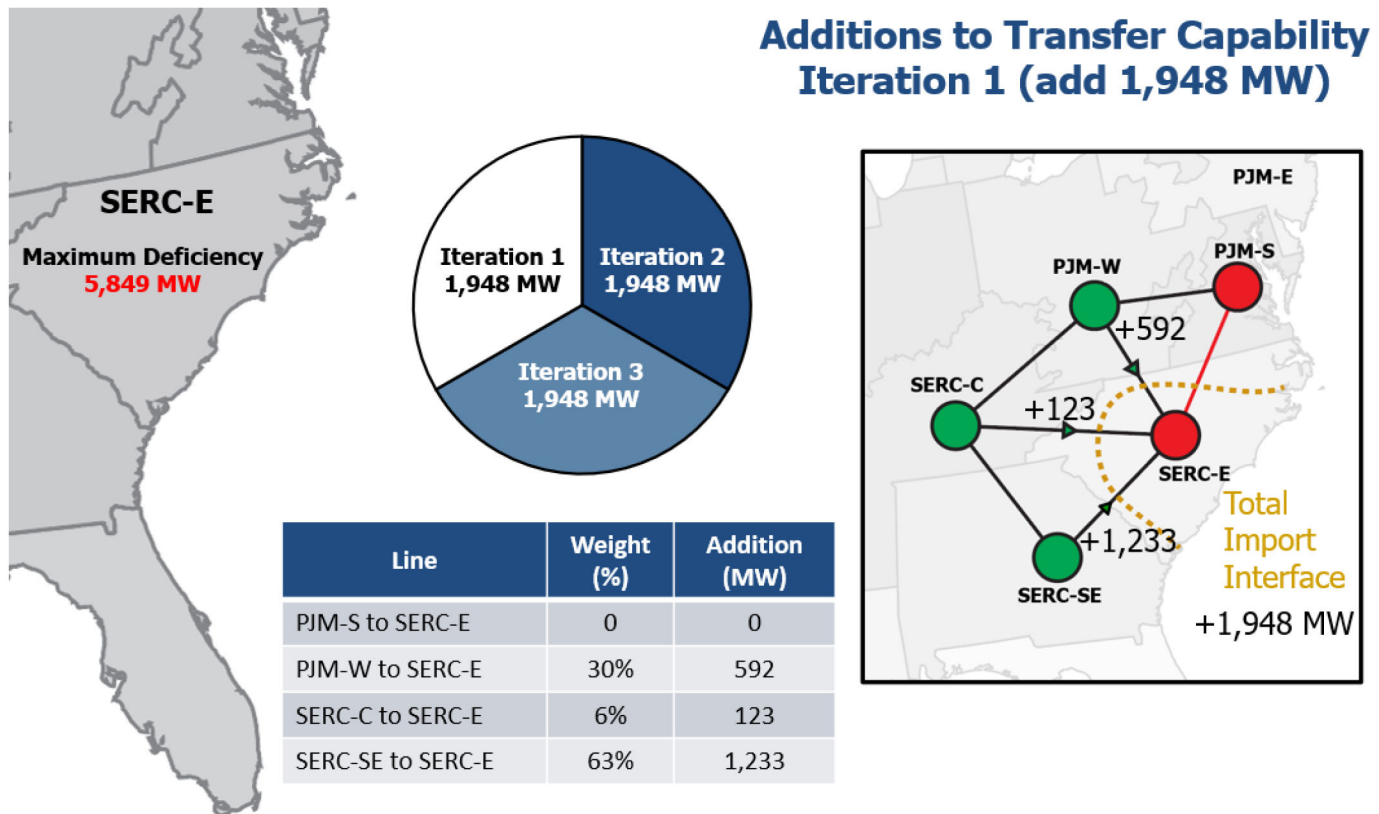


### Allocate

## Step 4: Allocate Additional Transfer Capability

Step 4 focuses on programmatically allocating transfer capability increases to constrained interfaces to address the Maximum Resource Deficiencies (identified in Step 2), using the scarcity weighting factors (calculated in Step 3). Specifically, the model initially allocates transfer capability increases of one third (33.3%) of the maximum resource deficiency proportionally to interfaces based on the relative difference in scarcity weighting factors, thereby prioritizing neighboring TPRs with relatively more surplus energy available. This partial increase allows the modeling method to capture interactive effects between TPRs and iterative effects as resources are re-dispatched, including exhaustion of surplus resources.

Continuing with the SERC-E example from the previous steps, the maximum resource deficiency observed in the 2024 energy margin analysis is 5,849 MW. The initial increase to transfer capability is 1,948 MW, one third of that amount. Using the difference in the scarcity weighting factors between the exporting TPR and importing TPR from Step 3, this additional transfer capability is allocated 30% to PJM-W (592 MW), 6% to SERC-C (123 MW), and 63% to SERC-SE (1,233 MW), as shown in **Figure 6.6**.



**Figure 6.6: SERC-E Iteration 1 Allocation of Additional Transfer Capability (2033 Case)**



### Iterate

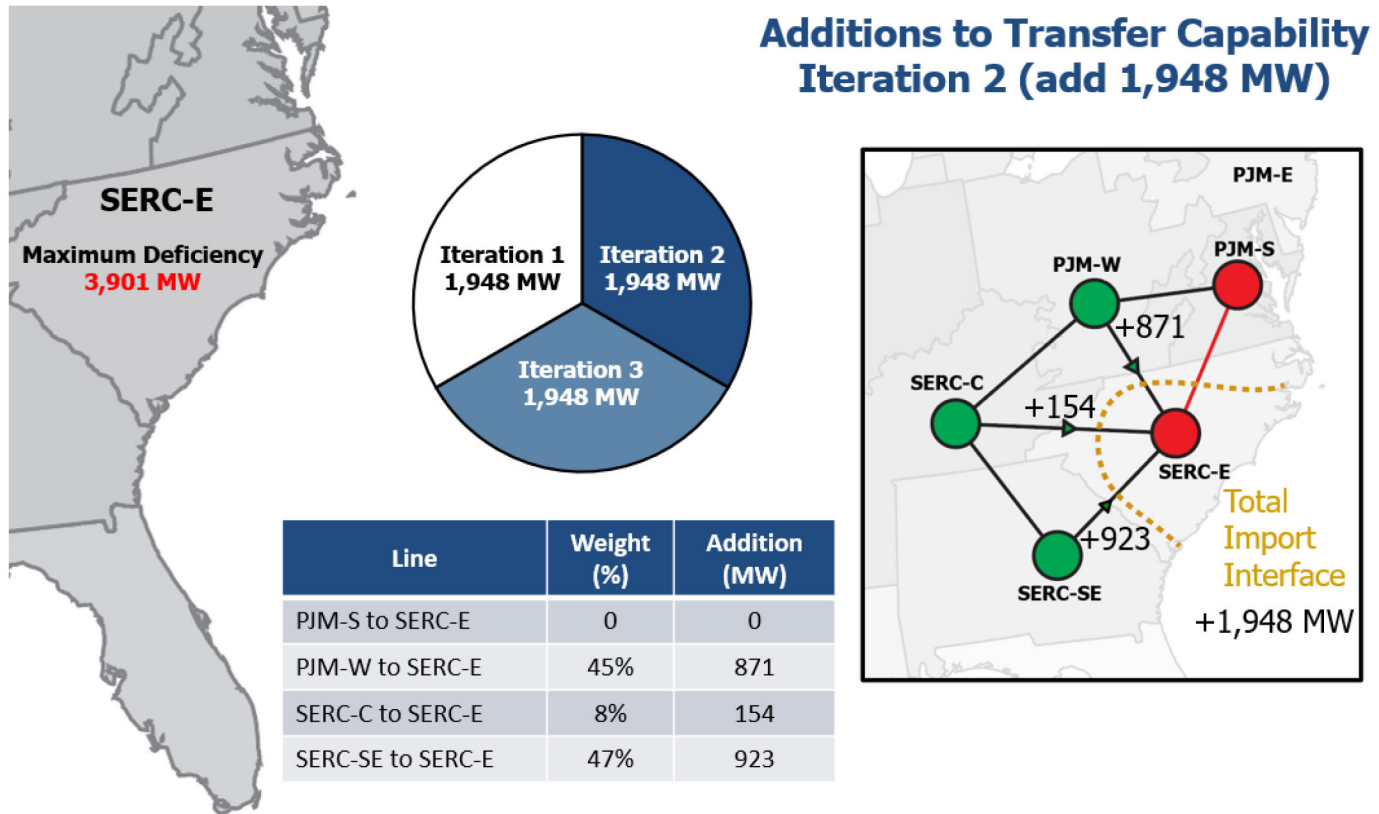
## Step 5: Iterate Until Resource Deficiencies are Resolved

Step 5 employs an iterative approach to incremental additions to transfer capability until all resource deficiencies are mitigated (if possible). The modeling method employed in Steps 1-4, including the energy margin analysis, is repeated with the increased transfer capability included.

The study repeated the process of adding transfer capability to constrained interfaces in blocks set at one third of the original maximum resource deficiency amount until all resource deficiency events were mitigated or until improvements stopped because there were no available resources from neighboring TPRs. This iterative approach ensures that the model accurately reflects the impact of each incremental change on the overall system, captures interactive effects, and allows for the finalization of prudent additions to be conducted after all modeling is complete rather than directly in the modeling process.

As shown in [Figure 6.7](#), after one iteration of additional transfer capability, the maximum resource deficiency decreased to 3,901 MW, a reduction of 1,948 MW. The second increase to transfer capability is again 1,948 MW (one third of the original maximum resource deficiency), but this time the allocation is 45% to PJM-W (871 MW), 8% to SERC-C (154 MW), and 47% to SERC-SE (923 MW), again based on the differences in scarcity weighting factors. This reflects tightening conditions in SERC-SE and is an intentional result of the iterative process.

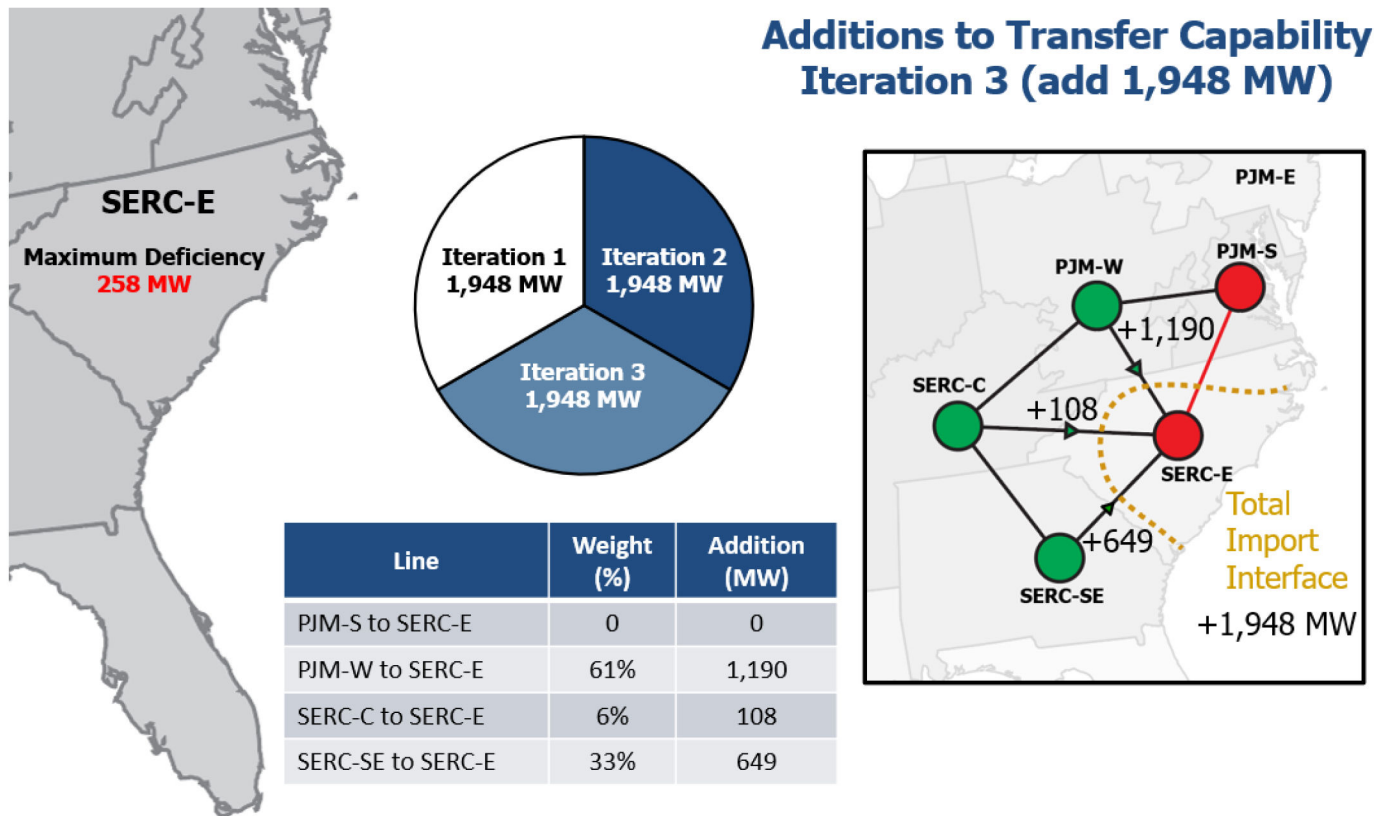




**Figure 6.7: SERC-E Iteration 2 Allocation of Additional Transfer Capability (2033 Case)**

As shown in [Figure 6.8](#), after two iterations of additional transfer capability, the maximum resource deficiency decreased to 258 MW, a further reduction of 3,643 MW, or 187% of the transfer capability added in Iteration 2, which is due to multiplier effects described in [Chapter 7](#). Despite the highly effective second iteration, there are still resource deficiency hours observed, so the process is repeated a third time. The third increase to transfer capability is again 1,948 MW (one third of the original maximum resource deficiency), and this time the allocation is 61% to PJM-W (1,190 MW), 6% to SERC-C (108 MW), and 33% to SERC-SE (649 MW) as surplus resources tighten in SERC-SE. Because of the highly effective second iteration, the programmatic third iteration size (1,948 MW) is larger than the remaining resource deficiency, and this will be adjusted proportionally in Step 6. After the third iteration, all maximum resource deficiency hours have been mitigated.





**Figure 6.8: SERC-E Iteration 3 Allocation of Additional Transfer Capability (2033 Case)**



## Finalize

### Step 6: Finalize Prudent Levels of Transfer Capability

Step 6 uses the results from the multiple iterations of Steps 1-5 described above. After completing all incremental modeling runs, the outputs were used to determine the recommended additions to transfer capability. This final step ensures that the recommendations are right-sized and effective, including identification of scenarios where additional transfer capability would not mitigate identified resource deficiencies. As a reminder, these recommended additions were based off the calculated 2024/25 current transfer capability values from Part 1, applied to the projected 2033 load and resource mix.

#### Prudent Additions Criteria

The following criteria<sup>89</sup> were applied when finalizing recommendations for prudent additions:

- Recommended additions were made to maintain a 3% minimum margin level,<sup>90</sup> if possible.
- Where practical, all resource deficiency hours were mitigated (i.e., there was no minimum threshold for the number of resource deficiency hours).
- While all resource deficiency hours were reported for each TPR, recommendations were only made to address resource deficiencies greater than 300 MW.<sup>91</sup>
- Recommended additions were rounded to the nearest 100 MW increment.
- Recommended additions address limiting interfaces and total import interfaces for the applicable season(s) where resource deficiency was identified.

<sup>89</sup> These criteria served as mechanisms to guide the application of sound engineering judgment so that prudent addition recommendations are reasonable. Since ITCIS is a reliability study, economic and policy objectives were not considered when making recommendations.

<sup>90</sup> This level was established based on an evaluation of average reserve requirements where load shed may occur.

<sup>91</sup> This criterion was derived from [EOP-004-4.pdf \(nerc.com\)](#) which prescribes thresholds for disturbance reporting.

- Where additions to transfer capability did not significantly reduce the resource deficiency, it was indicative of a lack of surplus energy in the source TPRs such that continued additions to transfer capability would have minimal benefit – additional transfer capability was considered prudent if it:
  - Reduced the maximum resource deficiency by at least 75% of the additional transfer capability, or
  - Reduced the resource deficiency by at least 100% of the additional transfer capability in at least four hours.

### Other Considerations for Prudent Additions

In addition to the criteria above, the following factors were considered:

- Recommended additions were only considered between neighboring TPRs.
  - Transfer capability additions that solely benefit a “neighbor’s neighbor” are outside the scope of this study, including the Part 1 analysis.
  - In cases where surplus energy in neighboring TPRs is insufficient to address the deficiency, supplemental reporting is included in [Chapter 7](#) regarding the nearest non-neighbor TPRs that could assist during resource-deficient hours.
- Recommended additions were prioritized from neighboring TPRs with relatively higher resource surplus, as measured by the difference in scarcity weighting factor discussed in Step 4.
- A 6% minimum margin level sensitivity was also reviewed.<sup>92</sup>
- Changes not reflected in the LTRA data, such as an announcement of delayed retirements, were not considered.
- Several generating units can connect to multiple Interconnections (non-simultaneously) without using the associated interface tie lines, thus they do not deplete the associated transfer capability. This capability should be considered as a potential reduction to the recommended additions and is noted where applicable.

### Example of Prudent Additions

Continuing with the 2033 SERC-E example, [Table 6.3](#) below shows the cumulative iterations of increases to transfer capability. Recalling that the remaining resource deficiency after Iteration 2 was only 258 MW, Iteration 3 was prorated to right-size the additional transfer capability. In accordance with the criteria above, these values were rounded to the nearest 100 MW. As a result, in this example, the prudent additions are 1,600 MW from PJM-W, 300 MW from SERC-C, and 2,200 MW from SERC-SE.

Table 6.3: SERC-E Finalizing Transfer Capability Additions (2033 Case)					
Iteration	Transfer Capability Additions (MW)				Max Resource Deficiency (MW)
	PJM-S	PJM-W	SERC-C	SERC-SE	
Base					5,849
Iteration 1	0	592	123	1,233	3,901
Iteration 2	0	871	154	923	258
Iteration 3*	0	155	14	84	0
Total	0	1,618	291	2,240	
Prudent**	0	1,600	300	2,200	

\*Prorated Based on Maximum Resource Deficiency

\*\*Rounded to Nearest 100 MW

<sup>92</sup> This sensitivity helped inform, for instance, if a TPR was very close to resource deficiency at 3% for a significant number of hours.

## Chapter 7: Prudent Additions (Part 2) Recommendations

### 2024 Energy Margin Analysis Results

The results of the energy margin analysis for the 2024 case are summarized in [Table 7.1](#), which provides an overview of the maximum resource deficiencies observed across various TPRs and weather years. This table illustrates how different TPRs perform using the 3% minimum margin level and identifying where resource shortfalls may occur under specific weather conditions. Note that these results include the ability of TPRs to share resources among each other, subject to resource availability and the current transfer capabilities quantified in Part 1. Blue highlighting indicates that the maximum deficiency occurred in the winter, while orange highlighting represents summer.

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Max Resource Deficiency
Washington	0	0	0	0	0	0	0	0	0	0	0	0	0
Oregon	0	0	0	0	0	0	0	0	0	0	0	0	0
California North	0	0	0	0	0	0	0	0	0	0	0	0	0
California South	0	0	0	0	0	0	0	0	0	0	0	0	0
Southwest	0	0	0	0	0	0	0	0	0	0	0	0	0
Wasatch Front	0	0	0	0	0	0	0	0	0	0	0	0	0
Front Range	0	0	0	0	0	0	0	0	0	0	0	0	0
ERCOT	0	0	0	0	0	0	0	0	2,669	10,699	7,585	8,354	10,699
SPP-N	0	0	0	0	0	0	0	0	0	0	0	0	0
SPP-S	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-W	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-C	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-S	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-E	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-C	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-SE	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-Florida	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-E	0	0	0	0	0	0	0	0	0	0	2,894	0	2,894
PJM-W	0	0	0	0	0	0	0	0	0	0	0	0	0
PJM-S	0	0	0	0	0	0	0	0	0	0	0	0	0
PJM-E	0	0	0	0	0	0	0	0	0	0	0	0	0
New York	0	0	0	0	0	0	0	0	0	0	0	1,242	1,242
New England	0	0	0	0	0	0	0	0	0	0	0	0	0

The analysis reveals that the 2024 case has relatively few resource deficiencies across most TPRs, indicating that, under the current system, there are sufficient resources and transfer capability in place to serve the load under the weather conditions and load levels evaluated. This outcome is significant because it suggests that the existing infrastructure is largely capable of maintaining energy adequacy across diverse scenarios except under especially challenging conditions. As such, the 2024 case serves as a valuable reference point for future comparisons, particularly when evaluating the 10-year out (2033) case. By establishing a baseline using the 2024 resource mix and load, the study can better assess how future changes in resource mixes, load growth, and extreme weather conditions might be impactful over the next decade. As a reminder, the simulations did not attempt to recreate actual operations or the resource mix from previous years. Instead, they applied the historical weather conditions from those years to the projected 2024 resource mix, providing insights into how the future system might respond to similar extreme events.

**The 2024 case was used for benchmarking, but the simulations did not attempt to recreate actual operations.**

One notable exception is that ERCOT exhibits resource deficiencies across multiple weather years. The most severe deficiency is observed during WY2021, coinciding with the extreme conditions of Winter Storm Uri. ERCOT faced a

maximum resource deficiency of approximately 10,700 MW after assuming improvements from winterization efforts.<sup>93</sup>

While Winter Storm Uri can be considered an outlier, the fact that ERCOT also experiences deficiencies in other weather years highlights a broader challenge. The ERCOT system, on average, reaches lower margin levels on a more regular basis than other TPRs. This vulnerability is partly attributable to ERCOT's limited transfer capability, which restricts its ability to import energy from neighboring TPRs during periods of high demand or supply shortages. This limited transfer capability underscores the importance of considering strategic enhancements to ERCOT's interregional connections to bolster its resilience against a variety of conditions. While ERCOT must be prepared to handle extreme conditions like Winter Storm Uri, this study highlights potential for increased transfer capability to address capacity deficiencies and avoid emergency measures, as an additional option along with internal resource additions and demand response.

In addition to ERCOT, other TPRs also show resource deficiencies, albeit on a smaller scale. For instance, New York experienced a deficiency during an early September heatwave in WY2023, while SERC-E encountered challenges during Winter Storm Elliott in WY2022. These instances highlight the potential vulnerabilities under specific extreme weather scenarios. Further details on the timing, size, and magnitude of these individual events are provided in **Chapter 9**, which provides a more granular, TPR-specific analysis.

While Canadian TPRs were included in the overall study, their results are not presented in this table. Instead, these findings will be detailed in a separate Canadian Report, ensuring that the unique characteristics and challenges of those TPRs are appropriately addressed.

In addition to the maximum resource deficiency, the total energy deficiency (GWh) and number of hours of deficiency provide insight into the 2024 case results. **Table 7.2** quantifies the total amount of resource deficiency on an energy basis (GWh) and **Table 7.3** provides the number of resource deficiency hours in each weather year, thus providing additional information on the size, frequency, and duration of events.

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<sup>93</sup> In the sensitivity case without winterization efforts, ERCOT's maximum resource deficiency reached approximately 25 GW, a shortfall that mirrors the scale of the actual Winter Storm Uri event.



**Table 7.2: Total Resource Deficiency (GWh) by TPR and Weather Year (2024 Case)**

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Avg
Washington	0	0	0	0	0	0	0	0	0	0	0	0	0
Oregon	0	0	0	0	0	0	0	0	0	0	0	0	0
California North	0	0	0	0	0	0	0	0	0	0	0	0	0
California South	0	0	0	0	0	0	0	0	0	0	0	0	0
Southwest	0	0	0	0	0	0	0	0	0	0	0	0	0
Wasatch Front	0	0	0	0	0	0	0	0	0	0	0	0	0
Front Range	0	0	0	0	0	0	0	0	0	0	0	0	0
ERCOT	0	0	0	0	0	0	0	0	4	167	19	44	20
SPP-N	0	0	0	0	0	0	0	0	0	0	0	0	0
SPP-S	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-W	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-C	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-S	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-E	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-C	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-SE	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-Florida	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-E	0	0	0	0	0	0	0	0	0	0	6	0	<1
PJM-W	0	0	0	0	0	0	0	0	0	0	0	0	0
PJM-S	0	0	0	0	0	0	0	0	0	0	0	0	0
PJM-E	0	0	0	0	0	0	0	0	0	0	0	0	0
New York	0	0	0	0	0	0	0	0	0	0	0	4	<1
New England	0	0	0	0	0	0	0	0	0	0	0	0	0

**Table 7.3: Annual Hours of Resource Deficiency by TPR and Weather Year (2024 Case)**

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Avg
Washington	0	0	0	0	0	0	0	0	0	0	0	0	0
Oregon	0	0	0	0	0	0	0	0	0	0	0	0	0
California North	0	0	0	0	0	0	0	0	0	0	0	0	0
California South	0	0	0	0	0	0	0	0	0	0	0	0	0
Southwest	0	0	0	0	0	0	0	0	0	0	0	0	0
Wasatch Front	0	0	0	0	0	0	0	0	0	0	0	0	0
Front Range	0	0	0	0	0	0	0	0	0	0	0	0	0
ERCOT	0	0	0	0	0	0	0	0	2	36	4	12	5
SPP-N	0	0	0	0	0	0	0	0	0	0	0	0	0
SPP-S	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-W	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-C	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-S	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-E	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-C	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-SE	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-Florida	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-E	0	0	0	0	0	0	0	0	0	0	5	0	<1
PJM-W	0	0	0	0	0	0	0	0	0	0	0	0	0
PJM-S	0	0	0	0	0	0	0	0	0	0	0	0	0
PJM-E	0	0	0	0	0	0	0	0	0	0	0	0	0
New York	0	0	0	0	0	0	0	0	0	0	0	7	<1
New England	0	0	0	0	0	0	0	0	0	0	0	0	0

The 2024 results provide a useful test case for the analysis, but ultimately are not used to recommend prudent additions. Instead, these recommendations were made based on the 10-year-out analysis, evaluating potential future resource mix and load levels in 2033.

## 2033 Energy Margin Analysis Results

The 2033 case analysis mirrors the 2024 analysis, but accounts for continued load growth, retirements, and new resource additions. The assumptions for load growth, retirements, and resource additions were based on projections

from the 2023 LTRA. Specifically in this case, all Tier 1 resources were added, plus additional Tier 2 resources where necessary to backfill retirements on an effective (accredited) capacity basis as described further in [Appendix E](#).

**Table 7.4** provides a detailed summary of the maximum resource deficiencies observed across different TPRs and weather years for the 2033 case. Like the 2024 results, the table quantifies the maximum resource deficiency observed in each TPR during each weather year, with the last column highlighting the maximum resource deficiency across all weather years. One difference between [Table 7.1](#) and [Table 7.4](#) is that purple highlighting indicates a weather year where resource deficiency hours were observed in both summer and winter.

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Max Resource Deficiency
Washington	0	0	0	0	0	0	0	0	0	0	0	0	0
Oregon	0	0	0	0	0	0	0	0	0	0	0	0	0
California North	0	0	0	0	0	0	0	0	0	0	3,211	0	3,211
California South	0	0	0	0	0	0	0	0	0	0	0	0	0
Southwest	0	0	0	0	0	0	0	0	0	0	0	0	0
Wasatch Front	0	0	0	0	0	0	0	0	0	0	0	0	0
Front Range	0	0	0	0	0	0	0	0	0	0	0	0	0
ERCOT	1,361	0	0	9,400	0	0	0	8,977	14,853	18,926	14,321	12,108	18,926
SPP-N	0	0	0	0	0	0	0	0	0	155	0	0	155
SPP-S	0	0	0	0	0	0	0	0	0	4,137	0	0	4,137
MISO-W	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-C	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-S	0	0	560	0	629	0	0	0	0	0	0	0	629
MISO-E	0	0	0	0	1,676	0	0	0	5,715	979	0	0	5,715
SERC-C	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-SE	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-Florida	0	0	1,030	1,152	0	0	0	0	0	0	0	0	1,152
SERC-E	0	0	0	0	0	0	0	0	0	0	5,849	0	5,849
PJM-W	0	0	0	0	0	0	0	0	0	0	0	0	0
PJM-S	0	0	0	0	0	0	0	0	0	0	4,147	0	4,147
PJM-E	0	0	0	0	0	0	0	0	0	0	0	0	0
New York	0	81	0	3,244	1,748	2,631	1,229	0	0	0	0	3,729	3,729
New England	0	0	0	85	0	984	68	0	0	0	0	0	984

In contrast to the 2024 case, the 2033 results indicate a more widespread challenge to energy adequacy, with additional TPRs exhibiting resource deficiencies and more weather years posing challenges. This is primarily due to tightening energy margins driven by load growth, the changing resource mix, and the application of current transfer capability to the future case.

In the 2033 case, 11 out of 23 TPRs are affected by resource deficiencies in at least one weather year, and in many cases, across multiple weather years. Eight of these TPRs had no deficiencies in the 2024 case.

Similar to the 2024 results, [Table 7.5](#) quantifies the total amount of resource deficiency on an energy basis (GWh) and [Table 7.6](#) provides the number of hours of deficiency in each weather year, thus providing additional information on the size, frequency, and duration of events.

Table 7.5: Total Resource Deficiency (GWh) by TPR and Weather Year (2033 Case)

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Avg
Washington	0	0	0	0	0	0	0	0	0	0	0	0	0
Oregon	0	0	0	0	0	0	0	0	0	0	0	0	0
California North	0	0	0	0	0	0	0	0	0	0	22	0	2
California South	0	0	0	0	0	0	0	0	0	0	0	0	0
Southwest	0	0	0	0	0	0	0	0	0	0	0	0	0
Wasatch Front	0	0	0	0	0	0	0	0	0	0	0	0	0
Front Range	0	0	0	0	0	0	0	0	0	0	0	0	0
ERCOT	2	0	0	19	0	0	0	37	201	668	91	57	90
SPP-N	0	0	0	0	0	0	0	0	0	<1	0	0	<1
SPP-S	0	0	0	0	0	0	0	0	0	55	0	0	5
MISO-W	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-C	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-S	0	0	1	0	1	0	0	0	0	0	0	0	<1
MISO-E	0	0	0	0	4	0	0	0	128	2	0	0	11
SERC-C	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-SE	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-Florida	0	0	2	2	0	0	0	0	0	0	0	0	<1
SERC-E	0	0	0	0	0	0	0	0	0	0	30	0	3
PJM-W	0	0	0	0	0	0	0	0	0	0	0	0	0
PJM-S	0	0	0	0	0	0	0	0	0	0	45	0	4
PJM-E	0	0	0	0	0	0	0	0	0	0	0	0	0
New York	0	<1	0	18	7	15	3	0	0	0	0	31	6
New England	0	0	0	<1	0	2	<1	0	0	0	0	0	<1

Table 7.6: Annual Hours of Resource Deficiency by TPR and Weather Year (2033 Case)

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Avg
Washington	0	0	0	0	0	0	0	0	0	0	0	0	0
Oregon	0	0	0	0	0	0	0	0	0	0	0	0	0
California North	0	0	0	0	0	0	0	0	0	0	17	0	1
California South	0	0	0	0	0	0	0	0	0	0	0	0	0
Southwest	0	0	0	0	0	0	0	0	0	0	0	0	0
Wasatch Front	0	0	0	0	0	0	0	0	0	0	0	0	0
Front Range	0	0	0	0	0	0	0	0	0	0	0	0	0
ERCOT	2	0	0	3	0	0	0	10	24	72	10	14	11
SPP-N	0	0	0	0	0	0	0	0	0	4	0	0	<1
SPP-S	0	0	0	0	0	0	0	0	0	34	0	0	3
MISO-W	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-C	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-S	0	0	2	0	2	0	0	0	0	0	0	0	<1
MISO-E	0	0	0	0	5	0	0	0	50	3	0	0	5
SERC-C	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-SE	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-Florida	0	0	4	2	0	0	0	0	0	0	0	0	<1
SERC-E	0	0	0	0	0	0	0	0	0	0	9	0	<1
PJM-W	0	0	0	0	0	0	0	0	0	0	0	0	0
PJM-S	0	0	0	0	0	0	0	0	0	0	20	0	2
PJM-E	0	0	0	0	0	0	0	0	0	0	0	0	0
New York	0	2	0	12	7	12	4	0	0	0	0	15	4.3
New England	0	0	0	1	0	3	1	0	0	0	0	0	<1

## Recommendations for Prudent Additions

As a result of the above analysis, additions to transfer capability are recommended as prudent for 10 TPRs as summarized in [Table 7.7](#) after following the six-step process described in [Chapter 6](#). The table is ordered from highest to lowest number of resource deficiency hours as observed in the study. Additional TPR-specific information can be found in [Chapter 9](#). Transfer capability additions did not fully resolve the identified resource deficiencies in California North and ERCOT.

Transmission Planning Region	Weather Years (WY) / Events	Resource Deficiency Hours	Maximum Deficiency (MW)	Additional Transfer Capability (MW)	Interface Additions (MW)
<b>ERCOT*</b>	Winter Storm Uri (WY2021) and nine other events	135	18,926	14,100	Front Range*** (5,700) MISO-S*** (4,300) SPP-S** (4,100)
<b>MISO-E</b>	WY2020 Heat Wave and two other events	58	5,715	3,000	MISO-W** (2,000) PJM-W (1,000)
<b>New York</b>	WY2023 Heat Wave and seven other events	52	3,729	3,700	PJM-E (1,800) Québec** (1,900)
<b>SPP-S</b>	Winter Storm Uri (WY2021)	34	4,137	3,700	Front Range** (1,200) ERCOT** (800) MISO-W (1,700)
<b>PJM-S</b>	Winter Storm Elliott (WY2022)	20	4,147	2,800	PJM-E (2,800)
<b>California North*</b>	WY2022 Heat Wave	17	3,211	1,100	Wasatch Front (1,100)
<b>SERC-E</b>	Winter Storm Elliott (WY2022)	9	5,849	4,100	SERC-C (300) SERC-SE (2,200) PJM-W (1,600)
<b>SERC-Florida</b>	Summer WY2009 and Winter WY2010	6	1,152	1,200	SERC-SE (1,200)
<b>New England</b>	WY2012 Heat Wave and two other events	5	984	700	Québec** (400) Maritimes (300)
<b>MISO-S</b>	WY2009 and WY2011 summer events	4	629	600	ERCOT*** (300) SERC-SE (300)
<b>TOTAL</b>				<b>35,000</b>	

\* Transfer capability additions did not fully address identified resource deficiencies

\*\*Existing interface is dc-only

\*\*\* Proposed new interface

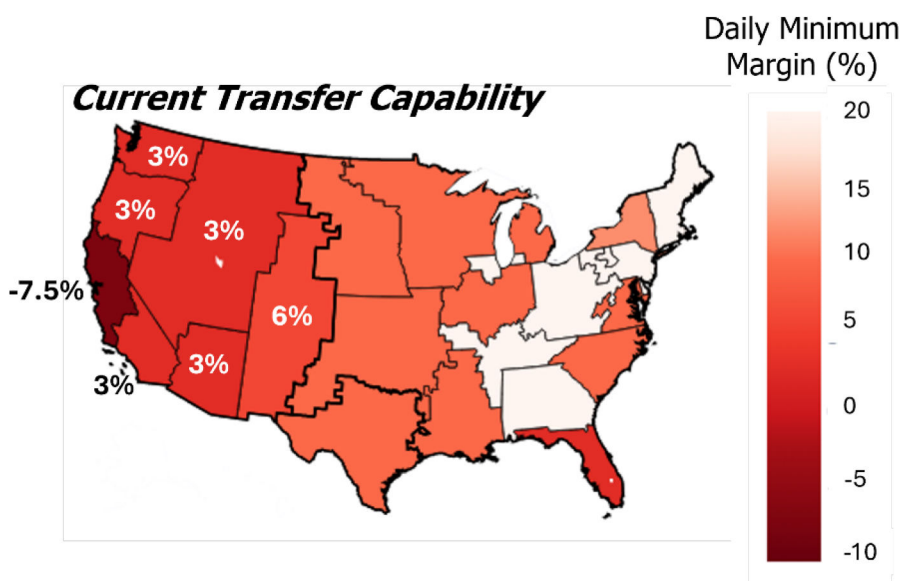
A further discussion of each TPR with prudent additions is provided below. Since these recommendations are based on current transfer capability (2024/25) as analyzed in Part 1, known planned projects likely to increase transfer capability are noted where applicable, and reviewed by the ITCS Advisory Group. This is not intended as an exhaustive list,<sup>94</sup> nor does it constitute an endorsement of any particular project; nevertheless, it illustrates that existing industry plans may be responsive to the recommended transfer capability increases.

**California North:** Recommendations are attributed to the 2022 heat dome that affected much of the Western U.S. where the energy margin analysis for California North showed resource deficiencies for a total of 17 hours over a

<sup>94</sup> Readers are encouraged to review available regional transmission expansion plans for a more complete list of planned projects.



four-day period. A prudent addition of 1,100 MW from Wasatch Front is recommended to help alleviate the resource deficiency. The proposed Greenlink project could help meet this transfer capability increase. However, during this same time, most of the Western Interconnection has low energy margins and all of California North's neighbors quickly reach their 3% minimum margin level, indicating that further increases in transfer capability would be ineffective in reducing resource deficiencies. In other words, there was a large-scale resource deficiency as shown in [Figure 7.1](#), such that neighboring TPRs could not mitigate the deficit. Additional transfer capability would be needed from non-neighboring systems further away, namely from Canada.



**Figure 7.1: Resource Saturation in the Western Interconnection, September 6, WY2022 (2033 Case)**

**ERCOT:** As noted in [Chapter 5](#), the energy margin analysis for ERCOT reflects a high level of plant winterization due to mandated improvements and compliance programs instituted by the state of Texas.<sup>95</sup> Notwithstanding, several instances of resource deficiency were also observed in both summer and winter seasons, the most severe of which was observed during WY2021 (Winter Storm Uri).

Even though neighboring TPRs (in particular, SPP-S and MISO-S) were also stressed during some of the same events, the study found that some surplus energy was available and additional transfer capability of 14 GW would be effective in resolving most of the identified resource deficiencies. Specifically, prudent additions from Front Range (5,700 MW), MISO-S (4,300 MW), and SPP-S (4,100 MW) are recommended, noting that connections to Front Range and MISO-S would be entirely new. Two substantial dc line projects have been proposed to increase transfer capability to and from ERCOT. One could transfer additional energy between Eastern Texas with the Eastern Interconnection, while the other would connect Western Texas with the Western Interconnection. Neither has reached the status to include in regional planning models but significant progress has been made.

**SPP-S:** Recommended additions for SPP-S were driven by WY2021 (Winter Storm Uri). Currently, simultaneous imports are limited to 6,400 MW. The prudent additions for SPP-S are for both individual lines and for the total import interface. The increases for individual transfer capabilities were from Front Range (1,200 MW), ERCOT (800 MW), and MISO-W (1,700 MW). The ability of generating stations to switch between SPP-S and ERCOT may at times address a portion of the need. Multiple projects approved in SPP's past Integrated Transmission Plans (ITP) have potential to increase transfer capability between SPP-N and SPP-S. In addition, SPP's 2024 ITP includes a proposal for two new

<sup>95</sup> A sensitivity analysis without this winterization assumption can be found in [Chapter 8](#).

345kV lines to address issues observed in its winter weather model which could further increase transfer capability across this interface.

**MISO-E:** Recommended additions for MISO-E were driven by three summer events in July and August for the 2011, 2020, and 2021 weather years. Summer events represent a high load risk due to extreme temperatures and potential low resource availability. Prudent additions are recommended for the summer months to increase transfer capability by 3,000 MW (2,000 MW from MISO-W and 1,000 MW from PJM-W), which would resolve the identified resource deficiencies. This increased transfer capability from MISO-W to MISO-E (2,000 MW) represents a substantial increase relative to the current transfer capability from MISO-W to MISO-E (160 MW). Some approved Tranche 1 projects in the MISO Transmission Expansion Plan have the potential to increase the transfer capability into lower Michigan.

**MISO-S:** Prudent additions for MISO-S were driven by two summer events in WY2009 and WY2011. Based on the energy margin analysis, additional transfer capability from ERCOT (300 MW) and SERC-SE (300 MW) would allow for access to surplus resources, resulting in part from load diversity during extreme summer heat events. The ability of the Frontier generating station to switch between MISO-S and ERCOT may address a portion of the need.

**SERC-Florida:** Prudent additions are driven by both summer (WY2009) and winter (WY2010) events. Since SERC-Florida is only a neighbor to SERC-SE, all recommended additions are between these two TPRs. The existing transfer capability to SERC-Florida from SERC-SE is 3,000 MW in the summer and 1,800 MW in the winter. An increase of 1,200 MW of transfer capability in both seasons resolves all resource deficiencies identified in the energy margin analysis. A planned relocation and reconductoring project may increase transfer capability somewhat, but stability limits will need to also be addressed to achieve the full 1,200 MW increase recommended.

**SERC-E:** Recommended additions for SERC-E are driven by WY2022 (Winter Storm Elliott) when the southeast United States saw extremely cold temperatures, high winter load, and decreased plant availability. Increased transfer capability of 4,100 MW from PJM-W (1,600 MW), SERC-SE (2,200 MW), and SERC-C (300 MW) would provide access to more resources during periods of high stress as Winter Storm Elliott moved across the southeast. These prudent additions resolve all resource deficiencies identified for SERC-E in the energy margin analysis.

**PJM-S:** Prudent additions for PJM-S are driven by WY2022 (Winter Storm Elliott) when the southeast United States experienced extremely cold temperatures, high winter load, and decreased plant availability. Additional transfer capability from PJM-E of 2,800 MW allowed for access to more resources in a TPR experiencing less severe extreme cold than PJM-S and resolved all PJM-S resource deficiencies.

**New York:** Prudent additions are driven by multiple summer events across weather years 2008, 2010, 2011, 2013, and 2023. The WY2023 event was the most severe, with several hours of resource deficiency across a three-day period while much of the northeast also experienced reduced energy margins. Additional transfer capability totaling 3,700 MW from PJM-E (1,800 MW) and Québec (1,900 MW) resolved all identified resource deficiencies. The planned Champlain Hudson Power Express is likely to address a significant portion of this need. The ability of the Beauharnois generating station to switch between Québec and New York may also address a portion of the need.

**New England:** Recommended additions for New England are driven by three summer events during weather years 2010, 2012, and 2013. Additional transfer capability of 700 MW, split between Québec (400 MW) and the Maritimes (300 MW), would provide access to TPRs not experiencing the same levels of high temperature and high load. The prudent additions for New England resolve all resource deficiencies identified in the energy margin analysis. The planned New England Clean Energy Connect project is likely to address a significant portion of this need.

## Other Key Insights

This section provides an in-depth analysis of the critical insights and conclusions drawn from Part 2 of the ITCS. These observations highlight several key topics that are essential for understanding the role of transfer capability in mitigating resource deficiencies. These include the following topics, each of which are explored in more detail below:

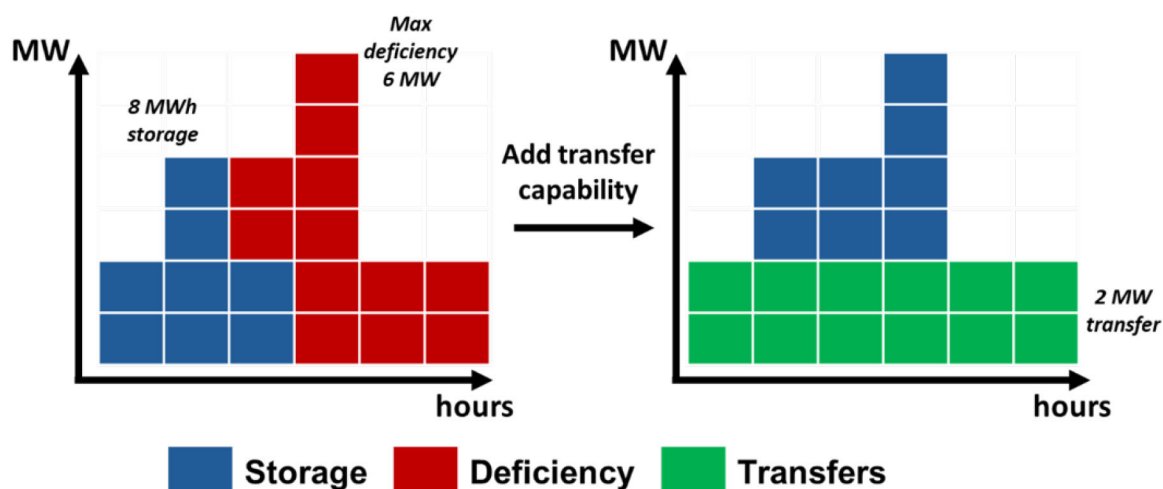
- Multiplier effects that may enhance the benefits of additional transfer capability
- Saturation effects observed when surplus resources in neighboring TPRs are exhausted
- The intricate relationship between generation and transmission planning
- Pronounced benefits of transfer capability across Interconnections
- Additional benefits that could be realized through “neighbor’s neighbor” transfer capability

## Multiplier Effects

Another key finding of the study is that increasing transfer capability can, at times, reduce the maximum resource deficiency by more than the transfer capability addition. For instance, a 1,000 MW increase in transfer capability can reduce resource deficiencies by more than 1,000 MW, as illustrated by the SERC-E example in [Chapter 6](#). While not immediately intuitive, this can occur for several reasons:

- **Storage Resource Optimization:** The additional transfer capability allows for pre-charging of storage resources, such as batteries and pumped storage hydro, that might not have been able to charge without the imports. This ensures that these resources, which otherwise would have been depleted, are available during future hours of resource deficiency. This is illustrated in [Figure 7.2](#).

**Additional transfer capability can optimize the effectiveness of existing storage resources.**



**Figure 7.2: Interactive Effects of Transfer Capability and Energy-Limited Resources**

- **Shortened Deficiency Windows:** Increased transfer capability can shorten the duration of resource deficiencies, by reducing the window from, for example, six hours to two hours. This enables energy-limited resources like batteries, pumped storage hydro, and demand response to manage the remaining hours more effectively.
- **Interactive Effects:** Transfer capability additions in one TPR can have cascading benefits for others. For example, an increase to transfer capability can help one TPR mitigate its own resource deficiency at one time but may also be used at other times to support a nearby TPR. Additionally, while the study primarily evaluated

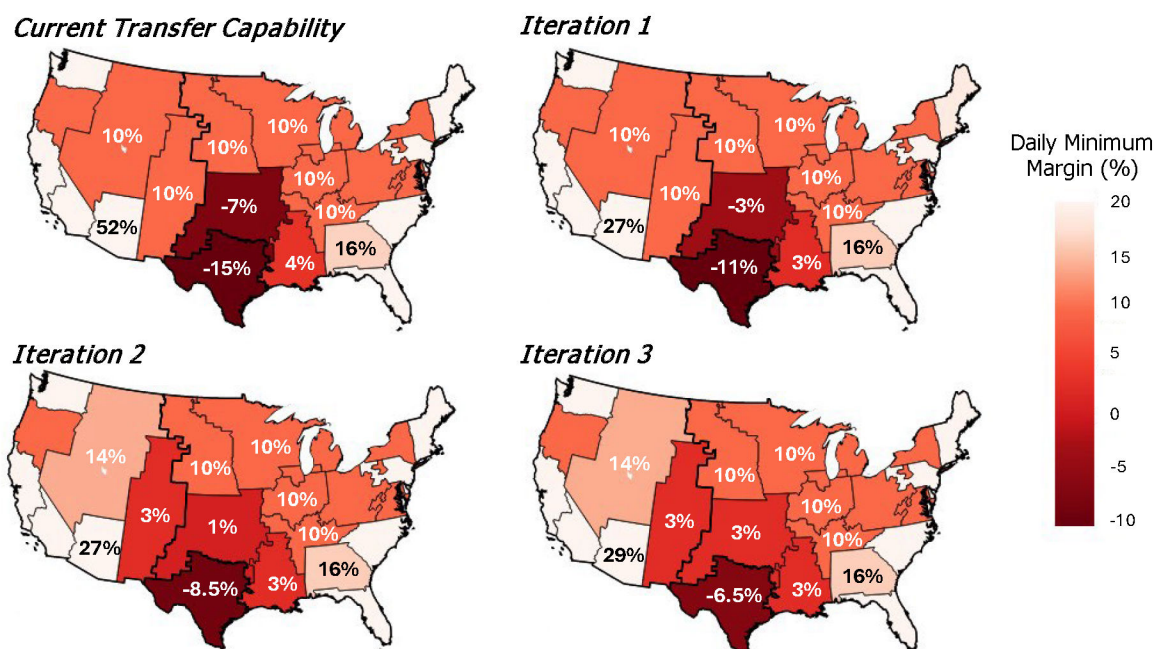


transfer capability in one direction, new transmission lines or upgrades could increase transfer capability in both directions, providing benefits to both sides of the transfer.

### Resource Saturation Effects

As discussed for the recommended additions for California North, the analysis demonstrated that increasing transfer capability can reduce observed resource deficiencies. However, it also revealed a point of saturation when the wider area exhausts its available resources. As neighboring TPRs run out of surplus energy to share, the benefits of additional transfer capability diminish. In such cases, the ability of additional transfer capability to mitigate resource deficiencies becomes limited, indicating that further mitigation would require different solutions, such as the introduction of new local resources or possibly a “neighbor’s neighbor” to access surplus energy. This saturation effect highlights the need for a more comprehensive approach to addressing resource deficiencies.

This saturation effect is most notable in ERCOT during Winter Storm Uri. [Figure 7.3](#) depicts the progressions of iterations of the 2033 case for one hour. In the starting case, some neighboring TPRs have surplus resources to share with ERCOT (hourly energy margins above the 3% minimum margin level). However, as transfer capability is added iteratively, these surpluses are exhausted. Eventually, additional transfer capability no longer substantially reduces resource deficiencies and is not deemed prudent.



**Figure 7.3: Resource Saturation Around ERCOT, February 16, WY2021 (2033 Case)**

### Relationship Between Generation and Transmission

The study found a nuanced but crucial relationship between generation and transmission. If multiple neighboring TPRs lack resources, additional transfer capability offers limited help because there is not enough surplus energy to share. Conversely, if TPRs each have surplus resources, the benefits of additional transfer capability are diminished, as each TPR can meet its own demands locally. Striking the right balance between generation and transmission to meet each TPR’s load is essential. However, it is important to consider that adding local resources to mitigate deficiencies may also have drawbacks as these new resources could be subject to the same constraints that caused the initial challenge, such as fuel supply restrictions or low renewable availability, leading to correlated risks. This finding points to the increased importance of holistic generation and transmission planning. This is particularly important as the resource mix changes and accelerated load growth is expected relative to the past decade. The ITCS evaluated the role of interregional transfer capability to improve energy adequacy reliability across different resource

mixes and study years and did not evaluate trade-offs between resource and transmission options. This is identified as an area of interest in the Future Work section later.

### Pronounced Benefits of Transfer Capability Across Interconnections

The study highlighted the significant benefits of transfer capability across Interconnections, where geographic diversity in resource availability and load proved advantageous. For example, the ties between SPP and the Western Interconnection demonstrated substantial benefits during extreme weather events. Similarly, transfer capability between ERCOT and both the Western and Eastern Interconnections provided crucial support, as does increasing transfer capability from Québec to New York and New England. Neighboring Planning Coordinators and Transmission Planners across Interconnections should continue to work toward a wider area planning approach.

### “Neighbor’s Neighbor” Transfer Capability Could Provide Additional Benefits

While the study focused on evaluating transfer capability between neighboring TPRs, the analysis suggests that additional benefits could be realized by improving transfer capability with a “neighbor’s neighbor” in two instances. Specifically, increasing transfer capability from ERCOT to SERC-SE or from British Columbia to California North could unlock access to even greater load and resource diversity, particularly during extreme events like Winter Storm Uri. TPRs two or more steps away from ERCOT had surplus energy available, as shown in [Table 7.8](#), even when ERCOT’s immediate neighbors were operating at their 3% minimum margin level.

Table 7.8: Energy Margins of Nearest TPRs During Resource Saturation (ERCOT)	
Transmission Planning Region	Average Energy Margin
SERC-SE	46%
Southwest	45%
Wasatch Front	22%
SERC-C	11%

Similarly, California North’s neighbors quickly depleted their surplus energy during the 2022 Western Heat Wave, but more distant TPRs still had surplus energy available, as shown in [Table 7.9](#). In particular, the Canadian provinces of British Columbia and Alberta had significant surplus during this event.

Table 7.9: Energy Margins of Nearest TPRs During Resource Saturation (California North)	
Transmission Planning Region	Average Energy Margin
British Columbia	57%
Alberta	46%
SPP-N	24%
Saskatchewan	16%

In summary, these results indicate that exploring and investing in “neighbor’s neighbor” transfer capability could provide a critical buffer during challenging grid conditions. However, the potential benefits of expanding connectivity to more distant TPRs must also be balanced with the associated costs and risks. These key findings underscore the importance of a balanced and strategic approach to enhancing transfer capability, recognizing both the strengths and limitations of existing infrastructure and the potential benefits of expanding connectivity to more distant TPRs.

## Chapter 8: Sensitivity Analysis

In addition to the 2024 and 2033 cases discussed in the previous sections, a series of sensitivity analyses were conducted to evaluate the impact of varying specific assumptions on the overall results. These sensitivities were designed to isolate the effects of individual factors and quantify their influence on resource deficiencies and the need for increased transfer capability. By examining these factors in isolation, the sensitivity analysis provides a clearer understanding of how changes in assumptions might alter the outcomes of the study. Each sensitivity was analyzed under both the current transfer capability and in scenarios with increased transfer capability to determine how recommendations might change.

The sensitivity analyses provide valuable insights into how different assumptions can influence study outcomes, including the necessity for enhanced transfer capability. By understanding these dynamics, future planning can be more responsive to a range of potential scenarios.

### ERCOT Winterization Effects

This section summarizes the effects of winterization on resource deficiencies in ERCOT. As discussed in [Chapter 7](#), the energy margin analysis included the anticipated effects of mandated winterization efforts in ERCOT to mitigate the impact of cold weather on thermal resource availability. [Table 8.1](#) through [Table 8.3](#) show the comparison between energy margin analysis results for ERCOT with and without these winterization assumptions.

**Table 8.1: ERCOT Maximum Resource Deficiency (MW) by Weather Year (2033 Case)**

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Max Resource Deficiency
ERCOT without Winterization	5,742	0	0	10,874	23,886	0	8,775	8,977	14,853	34,383	16,279	12,108	34,383
ERCOT with Winterization	1,361	0	0	9,400	0	0	0	8,977	14,853	18,926	14,321	12,108	18,926

**Table 8.2: ERCOT Total Resource Deficiency (GWh) by Weather Year (2033 Case)**

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Avg
ERCOT without Winterization	9	0	0	42	131	0	21	37	201	2129	102	62	228
ERCOT with Winterization	2	0	0	19	0	0	0	37	201	668	91	57	90

**Table 8.3: ERCOT Annual Hours of Resource Deficiency by Weather Year (2033 Case)**

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Avg
ERCOT without Winterization	3	0	0	7	11	0	3	10	24	148	11	15	19
ERCOT with Winterization	2	0	0	3	0	0	0	10	24	72	10	14	11

### 6% Minimum Margin Level Sensitivity

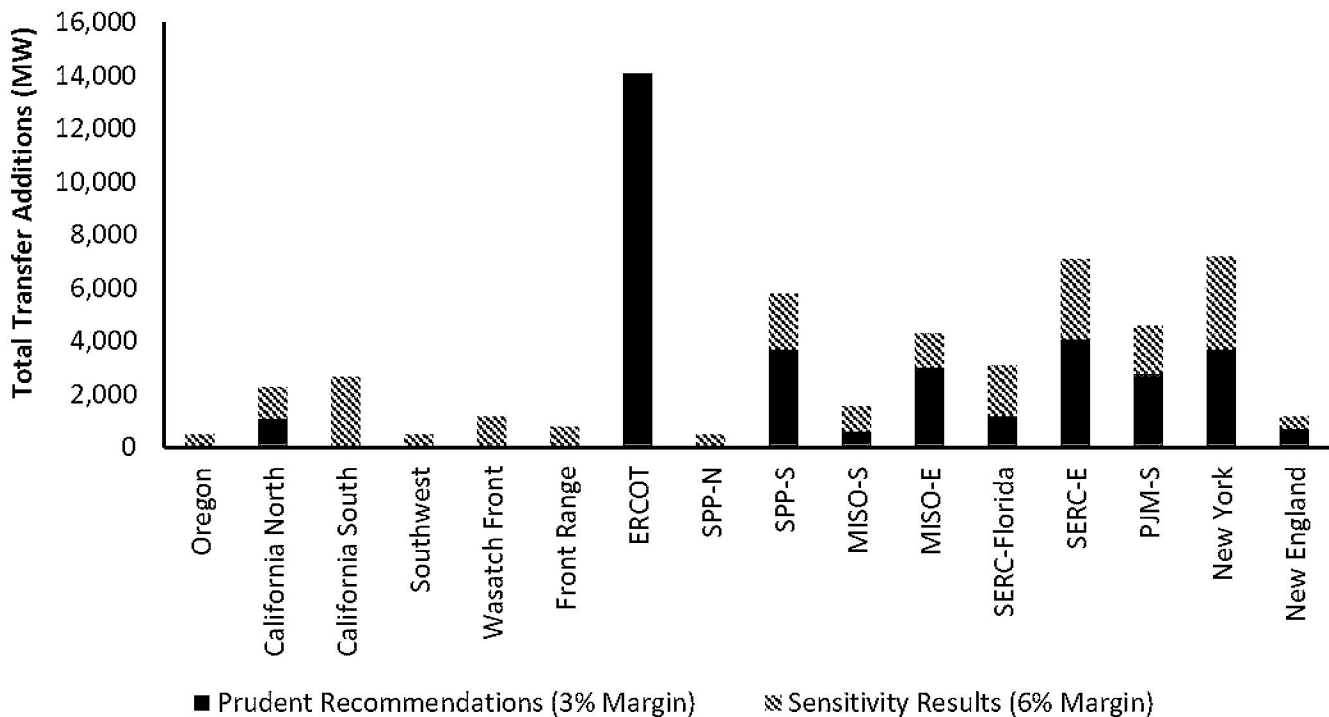
In this sensitivity analysis, the minimum margin level was increased from 3% to 6%, effectively reducing the surplus energy in all TPRs simultaneously. This adjustment led to an increase in the size, frequency, and duration of resource deficiencies, the number of TPRs experiencing these deficiencies, and the magnitude of transfer additions evaluated. [Table 8.4](#) compares the maximum resource deficiency between the 3% and 6% minimum margin levels. The 6% minimum margin level sensitivity introduces greater levels and frequency of resource deficiency for the 11 TPRs that showed resource deficiency in the 3% case and introduces resource deficiency in five additional TPRs. In particular, large portions of the Western Interconnection are simultaneously deficient, limiting the usefulness of additional transfer capability.



<b>Transmission Planning Region</b>	<b>Max Resource Deficiency (3% Margin)</b>	<b>Max Resource Deficiency (6% Margin)</b>	<b>Change in Max Resource Deficiency</b>
Washington	0	0	0
Oregon	0	1,626	1,626
California North	3,211	6,765	3,554
California South	0	7,984	7,984
Southwest	0	1,638	1,638
Wasatch Front	0	3,734	3,734
Front Range	0	2,190	2,190
ERCOT	18,926	21,391	2,465
SPP-N	155	639	483
SPP-S	4,137	5,362	1,225
MISO-W	0	0	0
MISO-C	0	0	0
MISO-S	629	1,677	1,049
MISO-E	5,715	6,410	694
SERC-C	0	0	0
SERC-SE	0	0	0
SERC-Florida	1,152	9,098	7,946
SERC-E	5,849	10,689	4,840
PJM-W	0	0	0
PJM-S	4,147	7,807	3,660
PJM-E	0	0	0
New York	3,729	5,953	2,224
New England	984	1,892	909

The iteration method described in [Chapter 6](#) was performed for the 6% minimum margin level sensitivity. While recommendations for prudent additions were not made based on this sensitivity, it highlights the importance of considering generation and transmission planning holistically along with benefits of potential “neighbor’s neighbor” transfers to mitigate resource deficiencies. This is because the more restrictive minimum margin level simultaneously reduces surplus resources for all TPRs, exacerbating resource deficiencies and reducing the effectiveness of existing and additional transfer capability. The results of the iterations for the 6% minimum margin level sensitivity in [Figure 8.1](#) reflect either where all deficiencies were resolved for a TPR, or where additional transfer capability was no longer beneficial due to saturation effects or lack of resources. No prudent recommendations were made based on these results and they should be viewed as exploratory only.

The cumulative additions across the United States increased from 35 GW of prudent additions to 58 GW in the case with a 6% minimum margin level. Notably, much of the Western U.S. now shows additions to transfer capability.



**Figure 8.1: Change to Transfer Capability Additions**

### Tier 1-Only Resource Mix Sensitivity

The analysis for the 2033 case included all announced retirements, Tier 1 resource additions, and a portion of additional Tier 2 resources if necessary to replace retiring capacity. In this sensitivity, no additional resources to replace retirements were included. In other words, this scenario reflected only the addition of Tier 1 resources, so significantly fewer resources were available to provide energy to serve existing load or support neighboring TPRs. As expected, this adjustment increased the frequency, duration, magnitude, and geographic distribution of resource deficiencies. **Table 8.5** shows the energy margin analysis by weather year results from this sensitivity, and **Table 8.6** shows the change in the maximum resource deficiency between the 2033 case and the 2033 Tier 1 Only case.

These results show that the buildout assumptions predominantly affect the Western Interconnection, where LTRA reporting included a large number of coal plant retirements, but the Tier 1 resources are insufficient, in isolation, to replace the capacity. These results also highlight that the risk is a clear resource adequacy issue, as each year in the historical record shows resource deficiencies, all of which are in the summer season. In this example, additional transfer capability between western TPRs will not improve energy margins as resource deficiency events often coincided across multiple TPRs.



Table 8.5: Maximum Resource Deficiency by Weather Year (2033 Tier 1 Only Case)

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Max Resource Deficiency
Washington	0	0	0	0	0	0	0	0	0	0	0	0	0
Oregon	0	0	2,550	1,114	144	1,022	1,534	1,666	1,573	398	1,864	3,959	3,959
California North	3,801	447	2,870	5,245	4,337	3,659	2,331	1,076	6,297	3,131	9,336	6,221	9,336
California South	9,791	1,520	6,622	10,387	8,664	11,690	5,562	7,549	6,301	509	11,768	5,408	11,768
Southwest	2,926	3,068	3,911	4,497	3,358	4,866	3,175	2,310	2,477	1,614	701	4,656	4,866
Wasatch Front	5,586	4,559	9,120	9,423	9,667	9,566	12,401	6,156	7,418	3,996	7,611	6,806	12,401
Front Range	2,584	2,086	3,940	5,353	6,054	4,686	4,298	4,087	2,987	3,180	3,231	5,728	6,054
ERCOT	9,964	0	7,158	10,088	0	0	0	13,628	15,431	19,511	16,171	16,519	19,511
SPP-N	0	0	0	0	0	0	0	0	0	155	0	0	155
SPP-S	0	0	0	0	0	0	0	0	0	4,137	0	0	4,137
MISO-W	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-C	0	0	0	0	0	0	0	0	0	0	0	0	0
MISO-S	0	0	3,637	0	3,910	1,800	2,550	0	0	0	1,237	93	3,910
MISO-E	2,533	0	3,173	3,815	5,046	3,479	0	3,626	6,924	5,363	1,392	779	6,924
SERC-C	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-SE	0	0	0	0	0	0	0	0	0	0	0	0	0
SERC-Florida	849	0	1,932	2,098	468	0	0	0	0	0	0	0	2,098
SERC-E	0	0	0	0	0	0	0	0	0	0	10,353	0	10,353
PJM-W	0	0	0	0	0	0	0	0	0	0	0	0	0
PJM-S	0	0	0	0	0	0	0	0	0	0	4,147	0	4,147
PJM-E	0	0	0	0	0	0	0	0	0	0	0	0	0
New York	0	81	0	3,244	1,748	2,631	1,229	0	0	0	0	3,729	3,729
New England	0	0	0	141	0	1,043	125	0	0	0	0	0	1,043

Table 8.6: Comparison of Maximum Resource Deficiency in 2033 (in MW)

Transmission Planning Region	Max Resource Deficiency (Rep. Retirements)	Max Resource Deficiency (Tier 1 Only)	Change in Max Resource Deficiency
Washington	0	0	0
Oregon	0	3,959	3,959
California North	3,211	9,336	6,126
California South	0	11,768	11,768
Southwest	0	4,866	4,866
Wasatch Front	0	12,401	12,401
Front Range	0	6,054	6,054
ERCOT	18,926	19,511	585
SPP-N	155	155	0
SPP-S	4,137	4,137	0
MISO-W	0	0	0
MISO-C	0	0	0
MISO-S	629	3,910	3,282
MISO-E	5,715	6,924	1,209
SERC-C	0	0	0
SERC-SE	0	0	0
SERC-Florida	1,152	2,098	946
SERC-E	5,849	10,353	4,504
PJM-W	0	0	0
PJM-S	4,147	4,147	0
PJM-E	0	0	0
New York	3,729	3,729	0
New England	984	1,043	60

By comparing the results of the 2033 case and the Tier 1 Only case the connection between resource and transmission planning is made apparent. When only considering Tier 1 resources, resource deficiencies worsen and affect larger portions of the country, often limiting the effectiveness of additional transfer capability. The “Replace Retirements” scenario was selected to represent an anticipated resource mix and highlight the role that transfer capability can play in improving energy adequacy.

As time progresses, the nature and severity of energy adequacy risks will evolve, thereby changing the effectiveness of transfer capability. This highlights the opportunities of periodic studies that evaluate future resource mixes across many hours of chronological load and resource availability as is done in this report.

## Chapter 9: TPR-Specific Results

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The following pages provide detailed results for each TPR, including information on each interface transfer capability, recommended prudent additions, information on each model iteration, assumed resource mix and peak load data, and details on resource deficiency events. Summary maps of transfer capability are also provided, with current transfer capability presented on the top, and recommended prudent additions highlighted in blue on the bottom. The map is provided for the season when transfer capability is required or for the peak demand season if there are no prudent recommendations. All data is provided for 2033 unless otherwise noted. Each of the following pages is organized as follows:

### Transfer Capability Summary Section

- Current summer and winter transfer capability columns include each of the interface names importing to the TPR summarized along with the summer and winter transfer capability quantified in Part 1.
- The prudent additions column provides the results of the simulations and the recommended additions to transfer capability for each interface.
- Recommended summer and winter transfer capability columns provide the TTC for each interface with prudent additions to the current transfer capability. Prudent additions are only added in the season(s) that they are needed to mitigate resource deficiencies.
- The total import interface limit represents the simultaneous import transfer capability determined in Part 1, excluding any transfer capability on dc-only interfaces, which is added to the following line if applicable.
- The total import interface + dc-only interfaces limit is provided both in MW and normalized as a percentage of the TPR's 2033 peak demand.

### Energy Adequacy by Iteration Section

- This section provides information on each iteration of the simulation, whether or not transfer capability was added for the respective TPR. In general, the energy adequacy metrics will improve in each iteration.
- Interchange hours represent the number of hours that the TPR imports from its neighbors in order to meet the 10% tight margin level. It is normalized by the total number of hours evaluated.
- Tight margin hours and resource deficiency hours quantify the total number of hours with tight margins (<10%) and resource deficiencies, respectively, after accounting for available transfers from neighbors. This is the total number of hours for all 12 weather years.
- Max resource deficiency represents the largest resource deficiency during the 12 weather years.
- Total deficiency is the total GWh of resource deficiency across the 12 weather years.

### Capacity and Load Data Section

- Resource capacity is presented for 2024 and 2033 by resource type. Thermal capacity includes coal, nuclear, single-fuel gas, dual-fuel gas, oil, biomass, geothermal, and other fuels. Variable renewable resources includes land-based wind, offshore wind, utility-scale solar, and behind-the-meter solar. Energy limited resources include pumped storage hydro, battery storage, and demand response.
- Winter capacities are provided for all thermal and hydro capacities. Nameplate capacity is provided for variable renewable and energy limited resources.
- Summer and winter peak demand is provided for 2024 and 2033 and represents the median peak demand, inclusive of behind-the-meter solar resources, but prior to demand response.

## **Resource Deficiency Events Section**

- The summary statistics for each day of resource deficiency in the base 2033 case is provided if applicable.
- Daily peak demand represents the day's highest load, regardless of when it occurs. Resource deficiency hours may occur before or after the peak demand hour due to variable renewable resources and energy limited resources having changing availability throughout the day.

Results for the following interfaces are presented in this chapter:

**Washington**

**Oregon**

**California North**

**California South**

**Southwest**

**Wasatch Front**

**Front Range**

**ERCOT**

**SPP-N**

**SPP-S**

**MISO-W**

**MISO-C**

**MISO-S**

**MISO-E**

**SERC-C**

**SERC-SE**

**SERC-Florida**

**SERC-E**

**PJM-W**

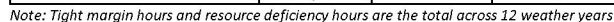
**PJM-S**

**PJM-E**

**New York**

**New England**

Note: The percentage of peak demand uses the higher of summer and winter 2033 peak load values

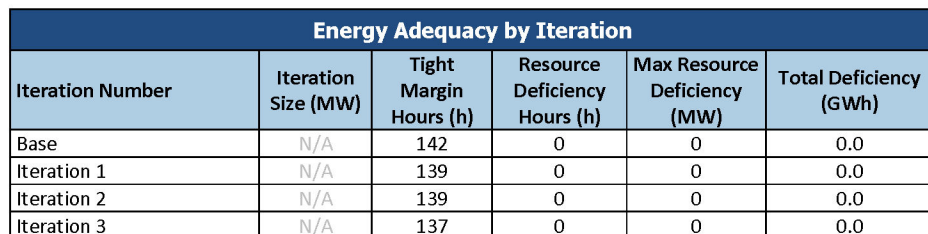


*Note: Thermal and hydro values represent winter ratings.*

*Note: Median peak demand across all weather years*

*Note: Daily peak demand does not necessarily reflect demand during resource deficiency hours*

Note: The percentage of peak demand uses the higher of summer and winter 2033 peak load values



Note: Tight margin hours and resource deficiency hours are the total across 12 weather years

*Note: Thermal and hydro values represent winter ratings.*

Note: Median peak demand across all weather years

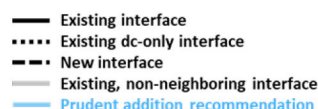
*Note: Daily peak demand does not necessarily reflect demand during resource deficiency hours*







*Note: The percentage of peak demand uses the higher of summer and winter 2033 peak load values*



*Note: Tight margin hours and resource deficiency hours are the total across 12 weather years*

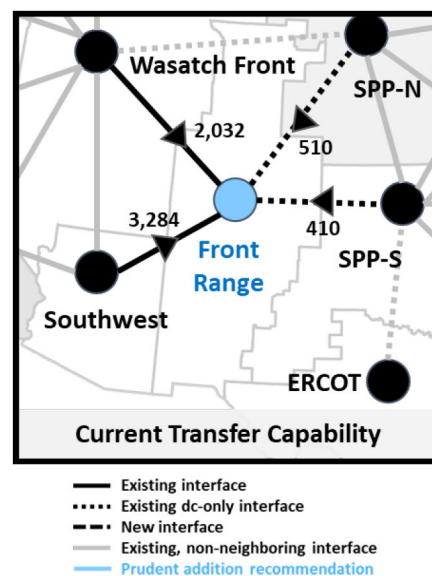
Note: Thermal and hydro values represent winter ratings

Note: Median peak demand across all weather years

*Note: Daily peak demand does not necessarily reflect demand during resource deficiency hours*



Note: The percentage of peak demand uses the higher of summer and winter 2033 peak load values



Note: Tight margin hours and resource deficiency hours are the total across 12 weather years

Note: Thermal and hydro values represent winter ratings.

*Note: Median peak demand across all weather years*

*Note: Daily peak demand does not necessarily reflect demand during resource deficiency hours*

ERCOT<sup>97</sup>

Total Transfer Capability (TTC) Summary

Interface Name	Current Summer (MW)	Current Winter (MW)	Prudent Additions (MW)	Recommended Summer (MW)	Recommended Winter (MW)
Front Range to ERCOT	Candidate	Candidate	5,700	5,700	5,700
MISO-S to ERCOT	Candidate	Candidate	4,300	4,300	4,300
SPP-S to ERCOT	820	820	4,100	4,920	4,920
Total Import Interface Limit	820	820	14,100	14,920	14,920
Total Import Interface Limit + dc-only Interfaces Limit	820	820	14,100	14,920	14,920
(as % of 2033 Peak Demand)	1%	1%	15%	16%	16%

Note: The percentage of peak demand uses the higher of summer and winter 2033 peak load values

Energy Adequacy by Iteration

Iteration Number	Iteration Size (MW)	Tight Margin Hours (h)	Resource Deficiency Hours (h)	Max Resource Deficiency (MW)	Total Deficiency (GWh)
Base	N/A	1520	135	18,926	1,074.7
Iteration 1	6300	271	30	13,976	192.5
Iteration 2	6300	116	12	9,486	53.0
Iteration 3	6300	66	3	7,828	17.1

Note: Tight margin hours and resource deficiency hours are the total across 12 weather years

Capacity and Load Data (in MW)

Resource Type	2024	2033
Thermal	73,557	74,750
Hydro	549	549
Variable Renewable	69,673	104,290
Energy Limited	13,586	24,951
Total	157,365	204,540

Note: Thermal and hydro values represent winter ratings

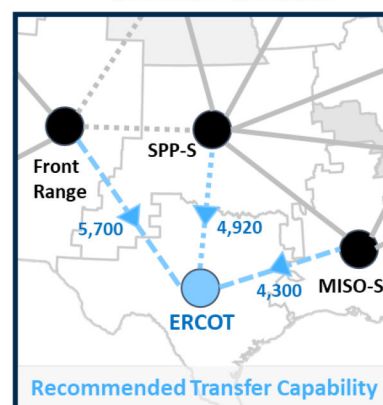
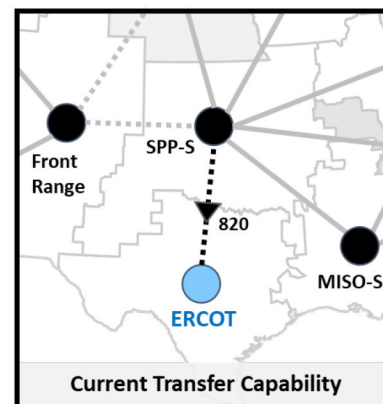
Summer Peak	84,059	92,214
Winter Peak	69,495	79,832

Note: Median peak demand across all weather years

Resource Deficiency Events

Event Date	Season	Daily Peak Demand (MW)	Max Deficiency Hours (h)	Total Deficiency (GWh)	Max Resource Deficiency (MW)
1/17 WY2007	Winter	78,063	2	1.9	1,361
1/9 WY2010	Winter	79,813	3	18.6	9,400
7/11 WY2019	Summer	90,223	3	16.8	8,977
7/12 WY2019	Summer	88,454	2	5.3	2,727
8/14 WY2019	Summer	93,169	2	6.4	5,150
9/22 WY2019	Summer	83,308	3	8.9	4,178
10/27 WY2020	Summer	67,078	20	177.3	14,853
10/28 WY2020	Summer	65,046	4	23.9	8,394
2/12 WY2021	Winter	81,982	6	63.2	12,556
2/13 WY2021	Winter	81,691	20	111.8	9,065
2/14 WY2021	Winter	88,567	11	96.6	14,513
2/15 WY2021	Winter	85,552	14	180.4	18,926
2/16 WY2021	Winter	83,137	13	142.2	14,198
2/17 WY2021	Winter	76,314	8	73.4	12,847
12/23 WY2022	Winter	88,897	3	38.3	14,321
12/24 WY2022	Winter	80,337	7	52.7	9,966
2/1 WY2023	Winter	76,242	5	17.9	6,305
8/24 WY2023	Summer	94,639	1	0.4	371
8/25 WY2023	Summer	94,402	4	22.7	12,108
8/26 WY2023	Summer	93,186	3	15.5	6,763
8/30 WY2023	Summer	87,334	1	0.5	481

Note: Daily peak demand does not necessarily reflect demand during resource deficiency hours



<sup>97</sup> Prudent additions include only iterations 1 and 2, plus a portion of iteration 3, due to resource saturation in neighboring TPRs. As a result, some resource deficiency hours were not resolved.













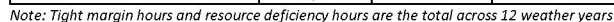








*Note: The percentage of peak demand uses the higher of summer and winter 2033 peak load values*

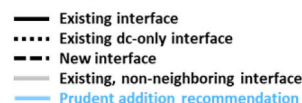


*Note: Thermal and hydro values represent winter ratings.*

*Note: Median peak demand across all weather years*

*Note: Daily peak demand does not necessarily reflect demand during resource deficiency hours*

Note: The percentage of peak demand uses the higher of summer and winter 2033 peak load values



*Note: Tight margin hours and resource deficiency hours are the total across 12 weather years*



*Note: Thermal and hydro values represent winter ratings.*

Note: Median peak demand across all weather years

*Note: Daily peak demand does not necessarily reflect demand during resource deficiency hours*













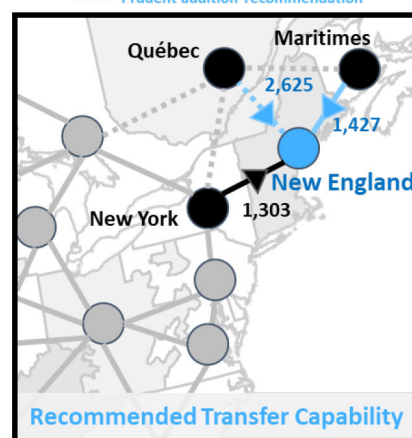
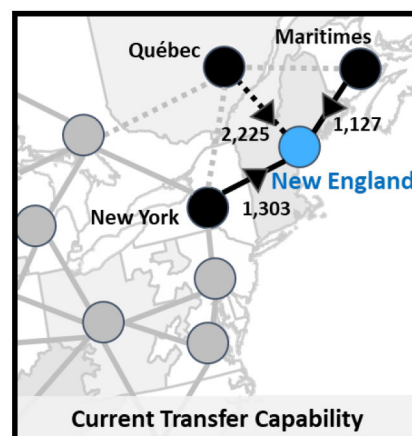




## New England

Total Transfer Capability (TTC) Summary					
Interface Name	Current Summer (MW)	Current Winter (MW)	Prudent Additions (MW)	Recommended Summer (MW)	Recommended Winter (MW)
Québec to New England	2,225	2,225	400	2,625	N/A
Maritimes to New England	1,127	1,265	300	1,427	N/A
New York to New England	1,303	2,432	0	1,303	N/A
Total Import Interface Limit	2,313	3,033	300	2,613	
Total Import Interface Limit + dc-only Interfaces Limit	4,538	5,258	700	5,238	
(as % of 2033 Peak Demand)	16%	18%	2%	18%	

Note: The percentage of peak demand uses the higher of summer and winter 2033 peak load values



Energy Adequacy by Iteration					
Iteration Number	Iteration Size (MW)	Tight Margin Hours (h)	Resource Deficiency Hours (h)	Max Resource Deficiency (MW)	Total Deficiency (GWh)
Base	N/A	146	5	984	2.4
Iteration 1	328	113	2	547	1.0
Iteration 2	328	80	0	0	0.0
Iteration 3	0	73	0	0	0.0

*Note: Tight margin hours and resource deficiency hours are the total across 12 weather years*

Capacity and Load Data (in MW)		
Resource Type	2024	2023
Thermal	26,567	26,377
Hydro	1,894	1,893
Variable Renewable	8,903	13,804
Energy Limited	2,784	2,796
Total	40,148	44,870

*Note: Thermal and hydro values represent winter ratings.*

Summer Peak	25,140	29,168
Winter Peak	20,552	26,829

*Note: Median peak demand across all weather years*

[illegible]

*Note: Daily peak demand does not necessarily reflect demand during resource deficiency hours*



## Chapter 10: Meeting and Maintaining Transfer Capability (Part 3)

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The third requirement in the Fiscal Responsibility Act of 2023 is to make recommendations to meet and maintain current transfer capability as well as the recommended additions.

As noted above, Part 2 of the ITCS recommended increases to transfer capability on particular interfaces as directed by the congressional mandate, but intentionally did not specify a particular set of projects or approach. This was intentional, as planners have multiple options for mitigating the identified energy adequacy risks. At a high level, these are:

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**Increased transfer capability is one of many options for addressing the identified energy deficiencies.**

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- Increase transfer capability to neighbors with surplus resources
- Construct local generation
- Increase demand response resources
- Accept the identified risks during extreme events (assuming other reliability thresholds are met).

The implementation time for these enhancements vary considerably, so depending on the options selected, grid operators must be prepared to maintain the reliability of the BPS through emergency measures, including rotating outages if necessary.

### Meeting Transfer Capability

If planners elect to increase transfer capability, there are multiple options to consider, including:

- Upgraded transmission infrastructure
- Remedial action schemes (RAS)
- Dynamic line ratings (DLR)
- Power flow control devices

The last two of these, along with advanced conductors, are frequently referred to as grid enhancing technologies. Grid enhancing technology projects are typically less expensive and require less lead time than building a new transmission line.

Regardless of the options chosen, planners need to perform detailed studies<sup>99</sup> to select projects and implement enhancements that will not result in other reliability issues. Increased transfers between TPRs can improve energy adequacy in some situations, but large transfers also have reliability implications that must be considered. When a large amount of energy is transferred, certain aspects of reliable system operations – such as system stability, voltage control, and minimizing the potential for cascading outages – must also be considered and mitigated, including the ability to withstand unplanned facility outages. This evaluation is crucial as an increased transfer capability may benefit neighboring TPRs under stressed conditions, but it can also potentially create reliability issues at other times if not mitigated.

Planners recognize that the thermal ratings of transmission lines may not be the most limiting constraint. Substation equipment may be more limiting than the transmission wires, so DLR or advanced conductors would not be effective without also upgrading the limiting elements. There may also be voltage limitations that can be remediated through

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<sup>99</sup> Transmission Planners and Planning Coordinators should consider both TPL-001 studies plus other study methods to review potential solutions to identified deficiencies.

capacitors or other reactive compensation devices. Finally, in some instances, there may also be stability constraints that need to be appropriately addressed. All solutions must be carefully coordinated between neighboring planners to avoid unforeseen third-party impacts.

### **Upgraded Transmission Infrastructure**

Building new and reconductoring existing transmission lines between TPRs are often effective options to increase transfer capability. Building new lines, either ac or dc,<sup>100</sup> between TPRs increases the ability to transfer energy, but this is typically a lengthy process, especially if new right-of-way is required.

Another way to increase transfer capability is to reductor existing transmission lines with conductors having higher ratings. Advanced high-temperature low-sag (HTLS) conductors use new materials and designs to increase the current-carrying capacity of transmission lines without significant sag, even at high temperatures. The operational characteristics of these conductors should be fully considered when evaluating potential applications.

In some cases, existing tower structures can be raised to provide additional ground clearance and thereby allow operation at a higher conductor temperature.

### **Remedial Action Schemes (RAS)**

In certain circumstances, it may be possible to increase transfer capability using a RAS. These schemes automatically respond to unplanned equipment outages when necessary to maintain operation within reliability criteria. The use of RAS must be planned, coordinated, and monitored to avoid unintended consequences. The use of RAS is generally discouraged as a long-term solution, as these schemes introduce higher levels of operational complexity, but may be helpful in the short term while other solutions are being implemented.

### **Dynamic Line Ratings (DLR)**

This technology uses real-time and forecasted weather conditions to continuously calculate the thermal capacity of transmission lines, typically based on a variety of factors.<sup>101</sup> At times it is possible to increase transfer capability by using higher facility ratings given lower temperatures and/or higher wind speeds. During favorable weather conditions, DLR can increase the transmission rating by 10-30%.<sup>102</sup> DLR can provide improved real-time visibility and customized equipment rating profiles.

However, DLR may not be suitable for addressing recommended additions in all situations, such as if the driving weather event was a summer event where temperatures are high and wind speeds are generally lower. Localized weather conditions are difficult to predict more than a day or two in advance, so planning studies beyond the operational time horizon may still need to rely on seasonal weather conditions to determine the facility ratings.

### **Power Flow Control Devices**

Power flow control devices, such as Flexible AC Transmission Systems (FACTS), Phase-Shifting Transformers (PST), and series compensation devices, are used to control and redirect the flow of electricity. This typically involves routing energy flows away from limiting constraints to optimize the use of existing transmission facilities without making changes to generator dispatch or topology. In general, FACTS have been in place for many years, but newer digital control technology allows for faster responses to system needs. This is especially of benefit in a loss of transmission or other contingency situation where these devices can quickly re-distribute power to maximize TTC. These devices could also be helpful in the integration of new renewable energy resources by using the existing capacity of the transmission system. Considering power flow control devices during the transmission planning process could allow for more options outside of transmission system expansion.

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<sup>100</sup> Because the Interconnections operate asynchronously, traditional ac solutions are unable to transfer energy between Interconnections.

<sup>101</sup> ERO Enterprise comments on FERC's advance notice of proposed rulemaking (ANOPR) were filed on October 15, 2024. See also [Reliability Insights](#) for more information on dynamic line ratings.

<sup>102</sup> <https://www.energy.gov/oe/articles/dynamic-line-rating-report-congress-june-2019>

## Maintaining Transfer Capability

The actual transfer capability available during real-time operations may be different from the calculated transfer capability, because system conditions during actual operation may be different from the studied conditions. A certain level of transfer capability cannot always be maintained due to changing system conditions, including planned maintenance and forced outages. Since it is not possible to always maintain a particular level of transfer capability in the operations horizon, this section focuses primarily on what can be done in the planning horizon.

### Future Studies

The data used in this study – including load forecasts, transmission topology, and resource mix – are constantly changing. NERC and the Regional Entities, working with industry, are planning to conduct regular assessments, rolled into future LTRA reports, that will consider the latest developments in resource mixes, transmission infrastructure, new load projections, and changing weather and climate patterns.

Planners can also evaluate changes in transfer capability as a part of regular planning processes, generator interconnection evaluations, and resource retirement studies. NERC encourages wide-area studies that holistically integrate transmission and resource planning.

Collectively, these studies can identify trends in interregional transfer capability and inform energy adequacy risk.

### Coordination Agreements

Strong coordination is important under normal and emergency operating conditions, but is particularly vital when the grid is stressed, such as during extreme weather events. Entities should ensure that coordination procedures are in place to maximize the support that can be reliably provided to help promote energy adequacy. This has been an important factor in minimizing the impact of recent events.

Effective interregional coordination of maintenance is also critical. The transmission system must be maintained, including rigorous operations and maintenance procedures, such as tree trimming and insulator washing, so that transmission lines are protected from some of the external factors that can contribute to faults which remove equipment from service on an unplanned basis, usually reducing transfer capability. Equipment maintenance must be planned to be performed outside of periods of increased system stress and coordinated with neighbors to avoid impacts to other systems. This applies to the interregional tie lines as well as many facilities internal to a region where an outage can impact neighboring systems.

## Regulatory or Policy Mechanisms and NERC Reliability Standards

The Fiscal Responsibility Act of 2023 requires FERC to post the ITCS report for public comments and subsequently submit a report to Congress including any recommended statutory changes. Such statutory changes could require entities to plan for recommended levels of transfer capability. As seen in the Part 2 analysis, a uniform minimum transfer capability requirement may not be necessary for some TPRs, nor a sufficient mechanism for others to ensure energy adequacy. Any statutory recommendations must ensure that the mandates result in actual transfer capability being available for entities to use under stressed system conditions.

Achieving the recommended levels of transfer capability may require upgrades to existing transmission facilities, as well as construction of new transmission facilities on new rights-of-way. ITCS recommends that policymakers consider implementing mechanisms to address current challenges with siting and permit approval processes, cost allocation methods, and multi-party operating and maintenance agreements, to accelerate the associated timelines where needed for reliability.<sup>103</sup>

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<sup>103</sup> A National Renewable Energy Laboratory (NREL) paper *Barriers and Opportunities to Realize the System Value of Interregional Transmission* can be found [here](#).

Currently, it is not NERC's intent to create a reliability standard for entities to establish a certain transfer capability. However, if events continue to occur or risks warrant such action, NERC may consider enacting reliability standards requiring certain assessments to be performed for planning transfer capability and appropriate mitigation measures put in place when risks to reliability warrant such action.

While there are no standards around transfer capability, there are standard development projects in progress around energy assurance. Project 2022-03 Energy Assurance with Energy-Constrained Resources and 2024-02 Planning Energy Assurance are meant to enhance reliability by requiring entities to perform energy reliability assessments to evaluate energy adequacy and develop corrective action plans to address any identified risks. These assessments will evaluate energy adequacy across multiple time horizons by analyzing the expected resource mix availability (flexibility) and the expected fuel availability during the study period. This standard is meant to address resource deficiencies that can result in insufficient amounts of energy on the system to serve electrical demand and impact BPS reliability.

The ERO Enterprise is also taking steps to help address this risk with its Energy Assessment Strategy that was developed in 2023. The purpose of this strategy is to enable assessments of reliability risk through the transition from a capacity-limited system to a more energy-limited system reliant on variable energy resources and natural gas-fired generators. The first major step in this strategy is implementing an annual probabilistic assessment with additional data, such as hourly demand and resource data and improved variable energy resource modeling.

## Chapter 11: Future Work

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While this study represents a pioneering and comprehensive effort to evaluate transfer capability and its impact on energy adequacy, it also had limitations due to the study's timeframe and there were lessons learned throughout the process. These factors highlight the need for additional future work to build on the findings and address areas that were not fully explored in this initial analysis. The following sections outline key areas for future work that will help refine and expand the understanding of transfer capability and its role in strengthening grid reliability.

### Explore Alternative Resource Mixes

One of the key areas for future work involves exploring alternative resource mixes to better understand the tradeoffs between generation and transmission options. By analyzing different combinations of generation types, such as varying levels of renewable energy integration and retirement of fossil fuel resources, a comparison can be made regarding the need for additional transmission infrastructure and generation resources. Future studies can offer more nuanced insights into how to optimally balance local generation with transfer capability. This exploration could help identify comprehensive strategies that also consider cost-effectiveness, policy objectives, and utility plans.

### Evaluate Transfer Capability Between “Neighbor’s Neighbor”

Another area for further study is the evaluation of transfer capability between non-neighboring TPRs, or “neighbor’s neighbors,” to capture additional reliability benefits and enhance geographic diversity. Connections such as ERCOT to SERC-SE and Front Range to California North, among others, represent opportunities to mitigate the resource saturation effects observed with immediately neighboring TPRs. While these connections may be more costly to build, they could provide significant benefits by extending the reach of surplus resources during extreme events, reducing the overall vulnerability of the grid, and may also access other benefits beyond reliability, like congestion savings or access to lower cost resources. Studies of this nature would require a wide area planning approach and cost allocation mechanism for any resulting system additions.

### Expand Weather Datasets

This study developed a consistent, time-synchronized weather dataset across wind, solar, load, and generator outages over 12 weather years. Some TPRs might not have shown deficits only because they did not experience a challenging weather event during the years that were evaluated. Similarly, another TPR may have experienced a resource deficit in the weather events analyzed, but there is no information regarding the future likelihood of these events. Expanding the analysis to include a more extensive dataset, including decades of historical and/or projected future weather data, would provide a more robust basis for evaluating investments.

### Evaluate Stability and Transfer Capability During Extreme Weather Events

Part 1 studies included power flow analysis, voltage screening, and known stability limits. Future studies should include more expansive stability analysis to identify potentially more restrictive limits, especially because stability limitations can become more prominent when there is increased reliance on heavy transfers across large areas.

Future work should also focus on evaluating transfer capability during extreme weather events. Part 1 results were based on summer and winter peak demand cases, but did not account for the specific weather conditions that led to resource deficiencies identified in Part 2. In subsequent studies, the power flow analysis should be dispatched based on the extreme weather events highlighted in the energy margin analysis. This approach will help determine whether the existing transfer capabilities calculated in Part 1 and assumed in Part 2 are practical and sufficient under real-world conditions and determine what, if any, additional mitigation may be needed to transfer energy up to the levels evaluated in this study.



## **Incorporate Probabilistic Resource Adequacy Analysis**

The methods and analysis in this study evaluated a single outage pattern for each weather year, incorporating weather-dependent outages and fuel supply disruptions. However, future work could expand this analysis to be fully probabilistic, considering hundreds or even thousands of outage scenarios rather than just 12 weather years. This expansion would allow for the estimation of probabilities and the introduction of typical resource adequacy metrics such as Loss of Load Expectation (LOLE), Loss of Load Probability (LOLP), and Expected Unserved Energy (EUE). These metrics would facilitate easier comparisons between transmission enhancements and generation resource additions, offering a more comprehensive view.

## **Establish Study Periodicity and Parameters**

To ensure that the findings and recommendations from this study remain relevant and adaptive to the evolving industry landscape, it is recommended that this type of evaluation be conducted on a regular basis. NERC and the Regional Entities, working with industry, are planning to conduct regular assessments, rolled into future LTRA reports, that will consider the latest developments in resource mixes, transmission infrastructure, new load projections, and changing weather and climate patterns. It is also recommended that NERC, working with industry, should promote consistency in how queue resources are categorized in reliability assessments. Additional sensitivities and alternative criteria may be explored.

Some differences in load forecasts and resource assumptions were noted when comparing study power flow cases to LTRA data. Standardizing case-building processes and associated content could ensure consistency and improve the efficiency of future studies.

There is also an opportunity to develop guidance for subdividing large areas and standardizing data sources for future studies. As the BPS evolves, the TPRs should be reviewed and modified as appropriate to identify significant limitations of interregional transfers. In a few instances where Balancing Authorities are split into multiple TPRs, there are opportunities to enhance available data to more efficiently account for each TPR, improving the data quality in future studies.

## Chapter 12: Acknowledgements

NERC appreciates the people across the industry who provided technical support and identified areas for improvement throughout the ongoing ITCS project.

**Table 12.1: NERC Industry Group Acknowledgements**

Group	Members
ITCS Executive Committee	Dave Angell (Industry Expert), Richard Burt (MRO), Charles Dickerson (NPCC), Tim Gallagher (RF), Fritz Hirst (NERC), Robert Kondziolka (Industry Expert), Mark Lauby (NERC), Gary Leidich (Industry Expert), Kimberly Mielcarek (NERC), Tim Ponseti (SERC), Sonia Rocha (NERC), Branden Sudduth (WECC), Joseph Younger (Texas RE)
ITCS Advisory Group	Gabriel Adam (IESO), Aaron Berner (PJM), Adria Brooks (DOE), Daniel Brooks (EPRI), Jessica Cockrell (FERC), Vandan Divatia (Eversource), Edison Elizeh (BPA), Robert Entriiken (EPRI), Vincent Fihey (Hydro Québec), Greg Ford (Georgia System Operations), Tom Galloway (NATF), Jeffrey Gindling (Duke Energy Midwest), Prabhu Gnanam (ERCOT), Biju Gopi (California ISO), Wayne Guttormson (SaskPower), Hassan Hayat (AEP), Matt Holtz (Invenergy), Larre Hozempa (FirstEnergy), Faheem Ibrahim (ISO New England), David Jacobson (Manitoba Hydro), Aubrey Johnson (MISO), David Kelley (SPP), Brett Kruse (Calpine), Darryl Lawrence (Pennsylvania Office of Consumer Advocate), Charles Long (Entergy), Chelsea Loomis (Northern Grid), Thanh Luong (FERC), Charles Marshall (ITC), Daryl McGee (Southern), Gayle Nansel (WAPA), Heidi Pacini (WestConnect), Colton Pankhurst (Natural Resources Canada), Nate Schweighart (TVA), Zachary Smith (NYISO), Lance Spross (ONCOR), Aidan Tuohy (EPRI), John Twitty (MJMEUC), Miguel Yanes (FP&L)
ITCS Transfer Study Team	Salva Andiappan (MRO), Diana Barsotti (NPCC), Kent Bolton (WECC), Edwin Cano (PowerGem), Bryan Clark (MRO), Vic Howell (WECC), John Idzior (RF), Marilyn Jayachandran (NERC), Gaurav Karandikar (SERC), Neeraj Lal (NPCC), Matthew A. Lewis (NERC), Saad Malik (NERC), Shirley Mathew (Texas RE), Melinda Montgomery (SERC), John Moura (NERC), Manos Obessis (PowerGem), Mohamed Osman (NERC), Shayan Rizvi (NPCC), Kevin Sherd (NERC), Paul Simoneaux (SERC), Doug Tucker (WECC), Dianlong Wang (MRO), Brad Woods (Texas RE)
ITCS SAMA Team (Scenarios, Assumptions, Metrics, and Adequacy)	Salva Andiappan (MRO), Diana Barsotti (NPCC), Richard Becker (SERC), Kent Bolton (WECC), Ryan Deyoe (Telos Energy), Matthew Elkins (WECC), Johnny Gest (RF), Vic Howell (WECC), Marilyn Jayachandran (NERC), Bill Lamanna (NERC), Matthew A. Lewis (NERC), Saad Malik (NERC), William Martin (NERC), Shirley Mathew (Texas RE), John Moura (NERC), Jack Norris (NERC), Mark Olson (NERC), Mohamed Osman (NERC), Matt Richwine (Telos Energy), Katie Rogers (WECC), Martin Sas (SERC), Kevin Sherd (NERC), Paul Simoneaux (SERC), Derek Stenclik (Telos Energy), Jim Uhrin (RF), Brad Woods (Texas RE)
ITCS Report Writing Team	Diana Barsotti (NPCC), Candice Castaneda (NERC), Bryan Clark (MRO), Mark Henry (Texas RE), Saad Malik (NERC), Stony Martin (SERC), Kevin Sherd (NERC), Robert Tallman (NERC), Jim Uhrin (RF), Brad Woods (Texas RE)

## Appendix A: Data Sources

The data sources used for the Part 2 analysis are shown in [Table A.1](#) below.

<b>Table A.1: Overview of the Two-Pronged Approach for Historical Weather Data</b>		
	<b>Synthetic Weather Data Weather Years 2007 - 2013</b>	<b>Scaled Historic Actuals Weather Years 2019-2023</b>
<b>Data Source</b>	North American meteorological datasets – often developed by National Labs, including National Solar Radiation Database (NSRDB), Wind Toolkit, etc.	Reported data from Balancing Authorities, including EIA-930 and FERC-714
<b>Historical Record</b>	Can span several weather years, typically 10-40 years, but current data gaps (specifically for wind resources) can limit years of analysis	Must use a shorter historical record, i.e., last three to five years, to make sure it is representative of current system
<b>Outlier Events</b>	Can get a longer history of outlier events (i.e., cold snaps in the 1980s) but estimates may be less accurate than recent observations	Fewer outlier events will be in the sample size (i.e., Winter Storm Uri, Elliott, heat domes) but may be more accurate than synthetic data
<b>Wind and solar profiles</b>	Captures geographic diversity based on new site selection and allows user to make assumptions on technology developments	Scaling historical generation amplifies correlation of resources and assumes technology remains constant
<b>Load Growth Trends</b>	Load data can be developed by end use to introduce changes from electric vehicles and building electrification	Embedded in the underlying load data, cannot be easily introduced
<b>Climate Trends</b>	Climate trends can be applied to underlying meteorological datasets	Embedded in the underlying data, cannot be easily introduced
<b>Application</b>	Better for analyzing future power systems and/or screening across a wider range of potential events	Better for analyzing near-term power systems during specific events

## Appendix B: Scaling Weather Year Load Profiles

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### Differences in the Synthetic and Historical Weather Year Data

Both the synthetic and historical weather year data have advantages and disadvantages, which is why two different datasets were used to extend the available weather years for analysis and to provide comparisons. The synthetic load supplements the fact that historical load may not capture changes in the underlying load shapes due to economic changes. Historical data supplements the need for reflecting actual conditions as they transpired and helps overcome challenges in acceptance for using purely synthetic data which relies on many assumptions. Both are useful for conducting the energy margin analysis and provide a wider picture of possible grid conditions.

### Historical Load

Before using the historical data in the study, it was necessary to clean and adjust it in the following ways:

- Clean data using data engineering practices:
  - Replace outlier load spikes (defined as load that is 4x median demand) with preceding or following hour demand.
  - Replace zero load reporting with interpolation or previous day's demand depending on duration of the events in EIA data.
  - Supplement EIA data with ISO-reported load for prolonged (multi-day) periods of reported zero or flat load in EIA 930 data.
- Add unserved energy (USE) back in for known events using the FERC, NERC, and Regional Entity Staff Reports for [Elliott](#), [Uri](#), and [CAISO's report on their 2020 event](#).
- Add estimates for behind-the-meter (BTM) generation that masks load.

### Synthetic Load

The synthetic load from NREL and EER represented "End Use Load" prior to reductions due to behind-the-meter solar (BTM PV) generation and does not include line losses. This means that the load factor of the synthetic weather year load is not altered by BTM PV, and no adjustments needed to be made to the hourly weather year profiles prior to scaling them to the LTRA forecasts.

### Target Forecast (2023 LTRA Annual Energy, Summer and Winter Peak Loads)

The target forecast for the study used the 2023 LTRA seasonal peak load and annual energy forecasts for 2024 and 2033 and assumed that these values represent the median forecast (P50). Based on this assumption, each set of weather year (synthetic and historical) loads were scaled so that the median peak and energy values of those datasets matched the values for each LTRA assessment area. The data provided in the LTRA forecast represents net energy for load which excludes the impacts of behind-the-meter PV. BTM PV was modeled as a supply side resource for the energy margin analysis, so the LTRA forecast was adjusted to gross load derived from BTM PV assumptions in the LTRA. The target peak and energy forecasts for each LTRA assessment area used in this study are shown in **Table B.1**.

**Table B.1: Adjusted LTRA Forecast Target Annual Energy and Summer/Winter Peak Loads**

Year	Period	ERCOT	MISO	New England	New York	PJM	SERC C	SERC E	SERC FL	SERC SE	SPP	WECC CA/MX	WECC NW	WECC SW
2024	Summer Peak (MW)	85,717	123,609	26,675	34,561	152,931	42,266	44,323	53,952	46,472	53,626	61,587	64,449	27,552
	Winter Peak (MW)	69,495	102,287	20,528	24,231	132,758	42,282	45,053	48,492	45,104	42,661	38,778	57,546	15,792
	Annual Energy (GWh)	469,383	682,261	128,773	160,663	814,833	225,229	231,307	261,337	243,058	299,150	287,384	381,958	127,379
2033	Summer Peak (MW)	96,163	128,270	31,202	37,834	165,476	43,122	48,333	61,396	48,055	59,265	74,285	79,232	32,878
	Winter Peak (MW)	79,946	105,562	26,723	31,552	145,120	42,764	47,549	52,954	47,523	48,383	45,638	68,103	19,731
	Annual Energy (GWh)	554,676	711,081	162,933	183,337	927,808	233,060	250,382	292,486	257,758	337,976	346,458	461,524	158,534

For the historical load, the EIA Form 930 served as the foundational dataset as it provides hourly loads at the Balancing Authority level along with sub-regional load for some ISO/RTOs. This sub-regional data was key for allocating load across the TPRs. EIA 930 provides demand as net generation for load values, the same as is reported in the LTRA.

For the synthetic load, data prepared for the National Renewable Energy Laboratory (NREL) Regional Energy Deployment System (ReEDS) model was used as the foundation for creating the 2007-2013 weather year load profiles for the TPRs. The underlying weather year dataset was prepared by Evolved Energy Research (EER) and purchased by NREL for several load growth scenarios. EER performs bottom-up load modeling and forecasts future loads based on building stock characteristics, industrial growth, electrification, etc.

The synthetic load scenario chosen for the study was the “EER\_Baseline\_AEO2022” dataset available on the NREL ReEDS-2.0 GitHub repository.<sup>104</sup> This load forecast represents business as usual load growth conditions based on projections from the Energy Information Administration's (EIA) 2022 Annual Energy Outlook. The load forecast was produced by Evolved Energy Research for the 2007 - 2013 weather years but represents consistent future economic years. This study used the forecasted load data for 2024 and 2033 and then adjusted peak and energy targets for the forecasts to align projections with the 2023 LTRA load forecast data.

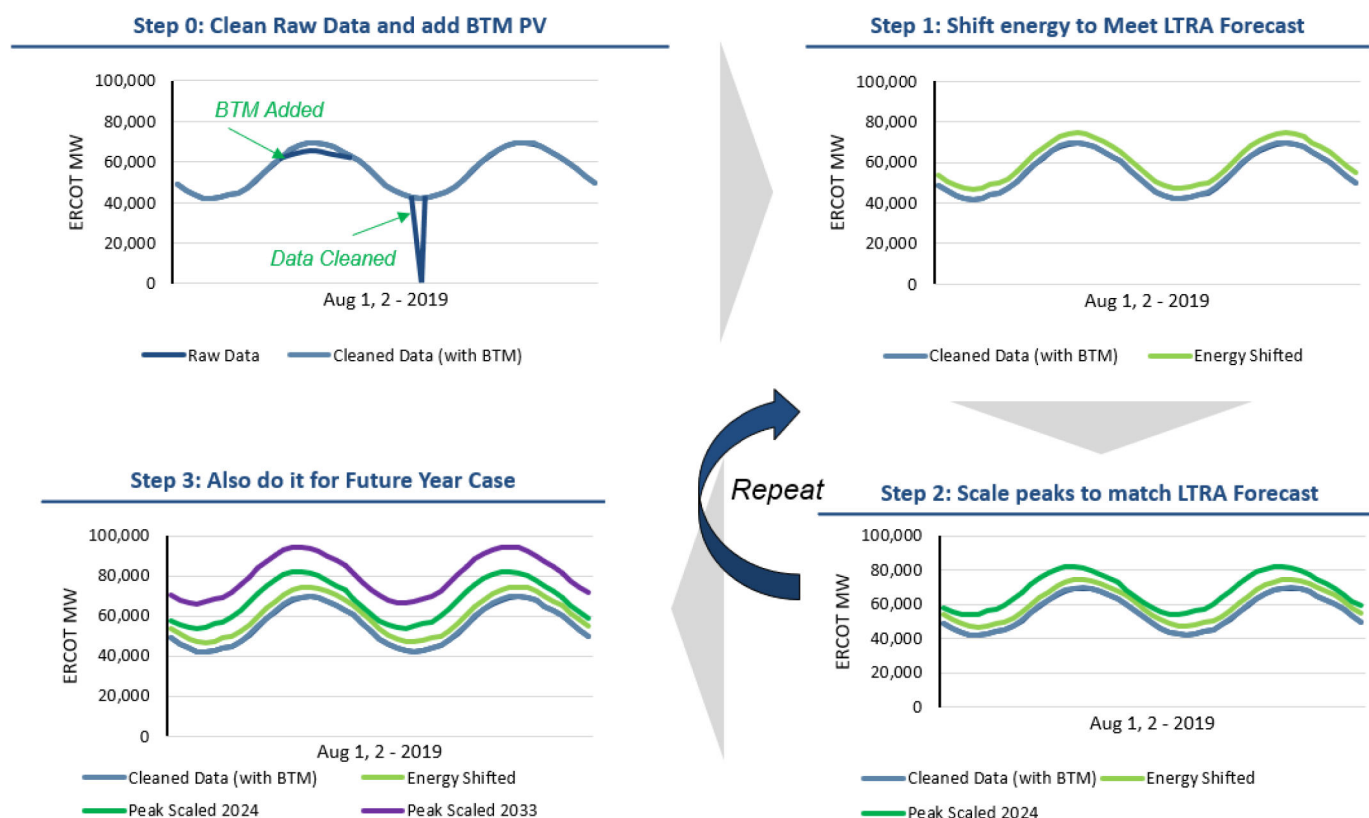
Both the synthetic and historical load profiles were scaled to align the median energy and peak loads from the weather years to the targets at the LTRA assessment area level. Adjusting just for energy targets can cause the peak load values to differ significantly from the target values in the LTRA forecast. This was accounted for by incrementally adjusting the hourly profiles so that the summer and winter median peak loads aligned with the forecast targets without changing the annual energy. This maintains variability in timing and magnitude of peak loads based on the weather and ensures that annual energy targets are maintained. The general steps taken to scale the load profiles are detailed below.

1. Add energy to each hour in a Weather Year so that the annual energy aligns with the LTRA forecast.
2. Adjust the energy shifted profiles to align the median weather year summer and winter peak loads with the LTRA forecast.
3. While maintaining the load shape, align scaled load with LTRA annual load factors.
4. Perform process for both 2024 and 2033 LTRA Forecast Years.

<sup>104</sup> NREL ReEDS-2.0, 2007-2013 weather year, see EER\_Baseline\_AEO2022, [GitHub - NREL/ReEDS-2.0](#)



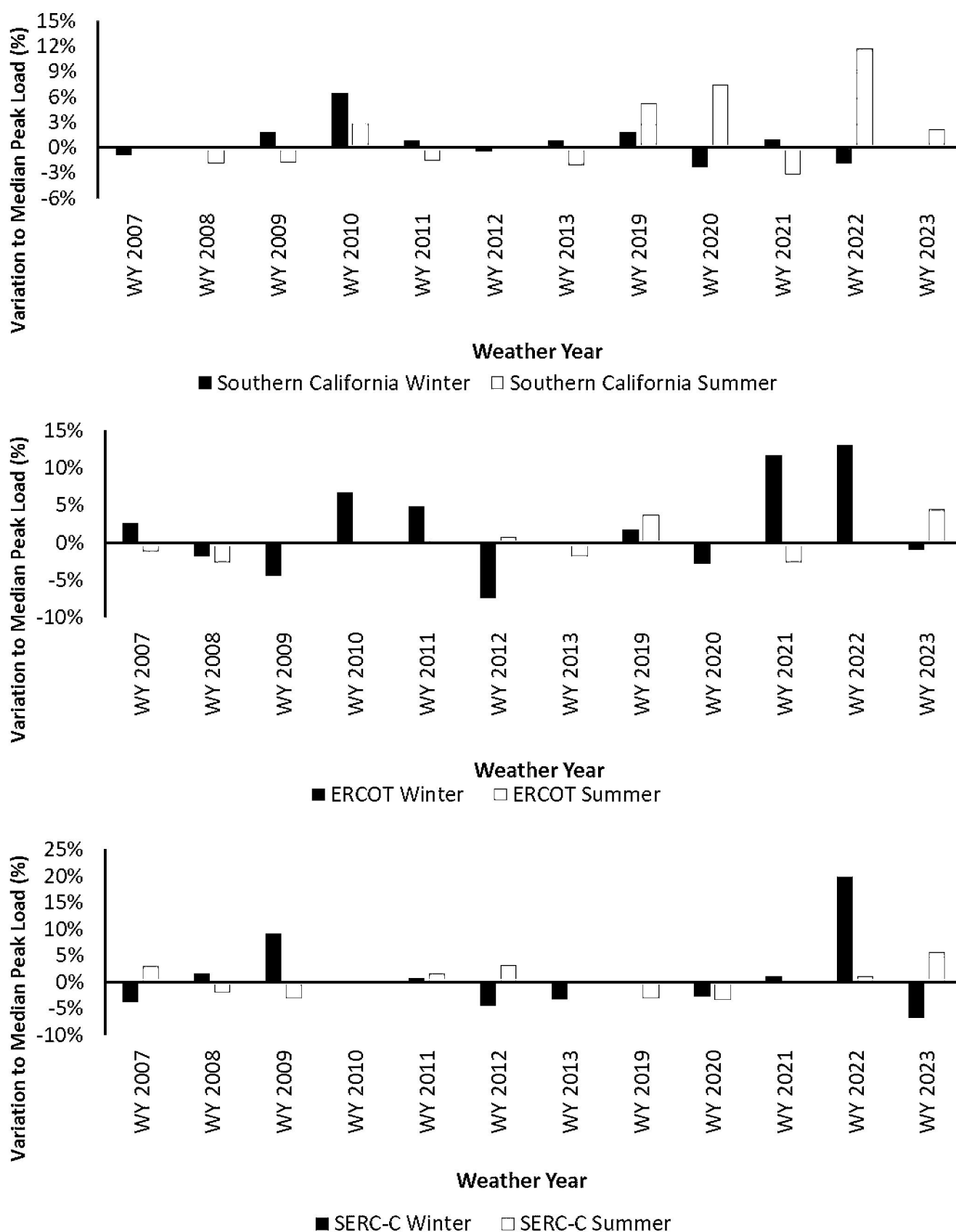
This process is portrayed graphically below as a historical data example. Step 0 for the historical data shows the cleaning and addition of BTM PV to the load profile (see [Figure B.1](#)).



**Figure B.1: Example of Load Scaling Process to Scale Weather Year Load Profiles to LTRA Forecast Years**

The load scaling step was done in reference to the LTRA assessment areas because these are the areas available in the LTRA forecast. After scaling the load data, each LTRA assessment area was disaggregated from an hourly LTRA profile into a TPR profile.

[Figure B.2](#) illustrates the variability in peak loads for three TPRs, namely California South, ERCOT, and SERC-C.

**Figure B.2: Weather Year Variation Relative to Median Peak Load for Selected TPRs**

## Appendix C: Annual Peak Load Tables by TPR

Annual peak loads for each TPR by weather year are shown in [Table C.1](#) and [Table C.2](#) below for the 2024 and 2033 cases, respectively. Annual peak loads vary due to the underlying weather conditions present for each TPR in each weather year. Minimum, median, and maximum annual peak load values are provided as a summary. Load reflects the net energy for load which excludes BTM PV.

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Min	Median	Max
Washington	18,294	19,358	20,226	19,178	17,835	17,371	19,356	20,071	18,390	19,370	20,674	19,379	17,371	19,356	20,674
Oregon	10,447	10,400	10,954	10,585	10,057	10,412	10,633	10,725	10,224	11,085	11,194	10,955	10,057	10,585	11,194
California North	23,972	23,468	23,913	25,219	24,281	24,910	24,000	25,658	25,067	24,174	28,324	25,016	23,468	24,281	28,324
California South	34,780	34,183	34,837	36,750	35,285	35,556	34,603	36,738	37,273	32,961	40,605	36,283	32,961	35,285	40,605
Southwest	21,085	21,295	21,965	21,814	21,066	21,260	21,194	20,613	21,856	22,317	21,345	22,345	20,613	21,295	22,345
Wasatch Front	26,109	25,178	25,135	25,515	25,304	25,982	26,774	23,815	24,798	25,625	25,750	25,089	23,815	25,304	26,774
Front Range	18,935	18,723	18,151	18,047	19,022	19,271	18,546	18,279	17,864	18,295	18,794	19,699	17,864	18,546	19,699
ERCOT	83,263	82,416	84,280	84,125	83,992	84,454	82,416	85,964	83,872	81,806	84,522	88,683	81,806	83,992	88,683
SPP-N	12,242	12,220	11,920	12,346	12,664	12,587	12,021	11,366	11,993	12,309	12,008	12,582	11,366	12,220	12,664
SPP-S	41,334	41,257	40,857	41,681	42,753	42,510	40,584	42,717	40,967	41,834	42,956	44,880	40,584	41,681	44,880
MISO-W	35,072	34,319	35,537	35,237	37,488	36,936	35,387	36,082	35,886	35,640	35,763	37,471	34,319	35,640	37,488
MISO-C	31,174	31,104	31,470	31,596	33,411	32,990	31,500	33,274	32,943	33,551	33,499	34,459	31,104	32,943	34,459
MISO-S	34,001	32,352	34,402	34,203	35,299	35,394	33,352	32,773	33,158	33,263	33,323	36,260	32,352	33,352	36,260
MISO-E	21,076	20,481	20,631	21,133	22,346	21,938	21,131	22,387	23,012	22,480	22,921	21,986	20,481	21,938	23,012
SERC-C	43,492	42,980	46,262	42,278	42,957	43,499	42,149	42,175	41,022	42,650	50,787	44,583	41,022	42,957	50,787
SERC-SE	47,799	46,567	48,226	47,197	47,713	47,020	43,314	46,017	46,226	46,346	47,944	46,749	43,314	46,749	48,226
SERC-Florida	53,968	53,277	55,269	58,856	53,131	52,986	53,161	51,820	51,262	53,636	53,893	55,964	51,262	53,277	58,856
SERC-E	45,051	44,926	46,882	45,247	45,856	45,091	42,604	46,337	44,978	44,062	51,628	44,922	42,604	45,051	51,628
PJM-W	77,282	75,819	74,440	75,468	81,135	78,745	78,649	77,980	78,920	79,319	78,243	76,039	74,440	77,980	81,135
PJM-S	35,670	33,929	34,262	35,559	38,358	38,173	37,520	38,703	37,162	36,542	39,664	38,831	33,929	37,162	39,664
PJM-E	35,390	34,043	33,781	35,455	38,432	38,821	37,307	39,076	38,153	38,719	37,868	38,843	33,781	37,868	39,076
New York	31,464	32,111	31,467	33,278	33,721	33,982	33,656	30,708	31,525	31,349	31,277	32,753	30,708	31,525	33,982
New England	24,490	25,102	24,830	26,286	26,928	26,423	26,700	24,143	25,179	25,562	24,919	24,843	24,143	25,102	26,928

Table C.2: Annual Peak Load by Weather Year (2033 Case)

Transmission Planning Region	WY2007	WY2008	WY2009	WY2010	WY2011	WY2012	WY2013	WY2019	WY2020	WY2021	WY2022	WY2023	Min	Median	Max
Washington	21,006	22,137	22,949	21,966	20,567	20,174	22,135	23,034	21,190	22,230	23,425	22,246	20,174	22,135	23,425
Oregon	12,144	12,028	12,671	12,329	11,658	12,093	12,384	12,333	12,124	13,254	12,922	13,237	11,658	12,329	13,254
California North	29,063	28,339	28,157	30,157	28,760	29,565	28,932	30,825	30,069	29,172	33,493	30,235	28,157	29,172	33,493
California South	42,969	42,235	42,911	44,947	43,221	43,740	43,126	42,866	43,647	39,401	48,448	43,430	39,401	43,126	48,448
Southwest	26,111	25,657	26,755	26,125	25,704	26,079	25,798	24,205	25,424	26,113	25,189	26,020	24,205	25,798	26,755
Wasatch Front	33,020	31,671	31,795	32,094	31,975	32,976	33,820	28,452	29,602	30,683	30,901	29,509	28,452	31,671	33,820
Front Range	22,371	22,365	21,466	21,635	22,864	23,381	22,347	21,681	20,853	21,266	22,199	23,101	20,853	22,199	23,381
ERCOT	90,619	90,490	92,160	91,393	92,268	92,619	90,062	96,792	92,312	90,391	92,947	96,638	90,062	92,160	96,792
SPP-N	13,531	13,502	13,157	13,632	14,010	13,909	13,280	12,638	13,308	13,660	13,343	13,959	12,638	13,502	14,010
SPP-S	45,686	45,587	45,099	46,027	47,301	46,980	44,839	47,153	45,285	46,182	47,369	49,362	44,839	46,027	49,362
MISO-W	36,466	35,616	36,912	36,576	39,013	38,396	36,738	37,513	37,310	37,063	37,191	38,934	35,616	37,063	39,013
MISO-C	32,453	32,279	32,742	32,838	34,811	34,312	32,756	34,597	34,243	34,869	34,803	35,757	32,279	34,243	35,757
MISO-S	35,345	33,564	35,720	35,493	36,724	36,845	34,615	34,038	34,421	34,532	34,613	37,606	33,564	34,615	37,606
MISO-E	21,908	21,250	21,422	21,936	23,250	22,804	21,932	23,215	23,850	23,311	23,754	22,800	21,250	22,800	23,850
SERC-C	44,374	43,338	46,580	43,105	43,796	44,475	42,872	42,643	41,557	43,116	51,141	45,481	41,557	43,338	51,141
SERC-SE	49,518	48,085	50,538	49,477	50,020	48,794	44,496	47,490	47,843	47,913	50,706	48,222	44,496	48,222	50,706
SERC-Florida	60,084	59,337	61,414	63,312	58,928	58,177	58,469	56,410	56,106	61,325	59,027	61,138	56,106	59,027	63,312
SERC-E	48,661	47,766	49,308	47,632	48,310	48,585	45,158	49,249	47,831	46,894	54,603	48,360	45,158	48,310	54,603
PJM-W	83,512	82,072	80,426	81,775	87,588	85,230	84,920	84,580	85,500	85,869	84,732	82,492	80,426	84,580	87,588
PJM-S	38,346	36,542	36,662	38,306	41,207	41,223	40,406	41,839	39,842	39,276	42,924	41,661	36,542	39,842	42,924
PJM-E	38,468	36,536	36,691	38,294	41,506	41,970	40,389	42,377	40,785	41,359	40,122	41,585	36,536	40,389	42,377
New York	34,285	35,149	34,406	36,429	36,792	36,725	36,798	33,270	33,624	33,088	32,223	34,679	32,223	34,406	36,798
New England	28,588	29,224	28,781	30,683	31,368	30,758	30,890	29,288	29,113	29,357	28,196	28,403	28,196	29,224	31,368

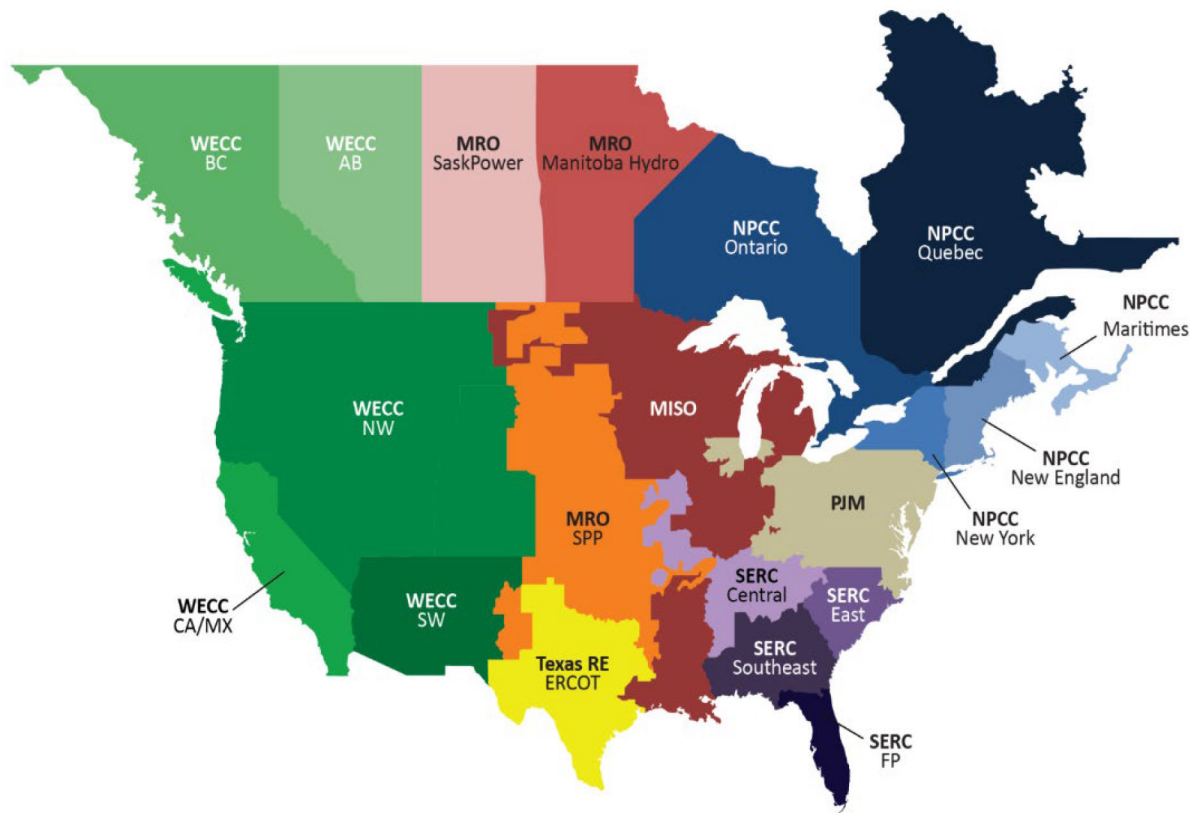
## Appendix D: Sub-regional Mapping

All the data used for the energy margin analysis was reported or developed at one of three levels, the LTRA assessment areas, the EIA Balancing Authority and sub-regional topology, or the NREL ReEDS topology. To reconcile data that was not aligned with the TPR topology, mapping between the different topologies was done. The figures in this section present the different topologies that were mapped to align data to both the LTRA assessment areas and TPRs, which are shown in [Figure D.1](#) and [Figure D.2](#), respectively.

Generators provided in the LTRA data form were mapped from LTRA assessment area to TPR based on several mapping rules listed in order of hierarchy below.

- LTRA maps one-to-one with the TPR. Examples are SERC-C, SERC-SE, SERC-E.
- Specific mappings based on supplemental data submitted in the LTRA such as Balancing Authority, data submitter, State, or Regional Entity review of select plants.
- Manual mapping for generators that could not be assigned using the first two approaches. Generator names, or interconnection numbers, were mapped to a TPR using EIA or interconnection queue data.

The results of this mapping exercise compared against the capacities in the power flows used in the Part 1 analysis is shown in [Figure D.3](#).



**Figure D.1: LTRA Assessment Areas (Resource Mix and Load Scaling Topology)**